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# Operational Reactor Safety

**22.091/22.903**

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Professor of the Practice

## Lecture 4

# Fuel Depletion & Related Effects



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# Topics to Be Covered

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- Fuel “burnup”
- Transmutation
- Conversion/Breeding
- Samarium 149
- Xenon 135
- Operational Impacts

# Fuel Burnup

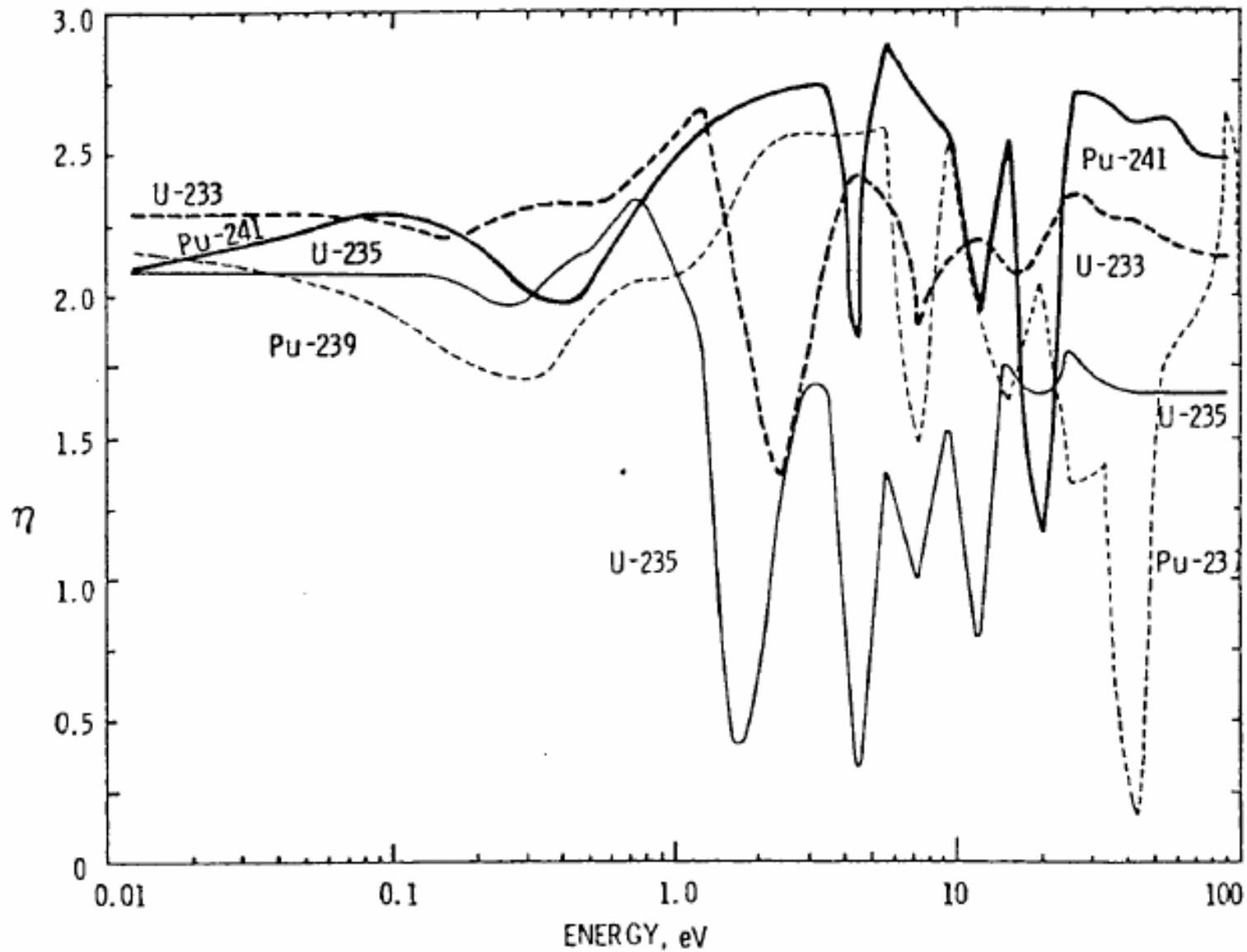
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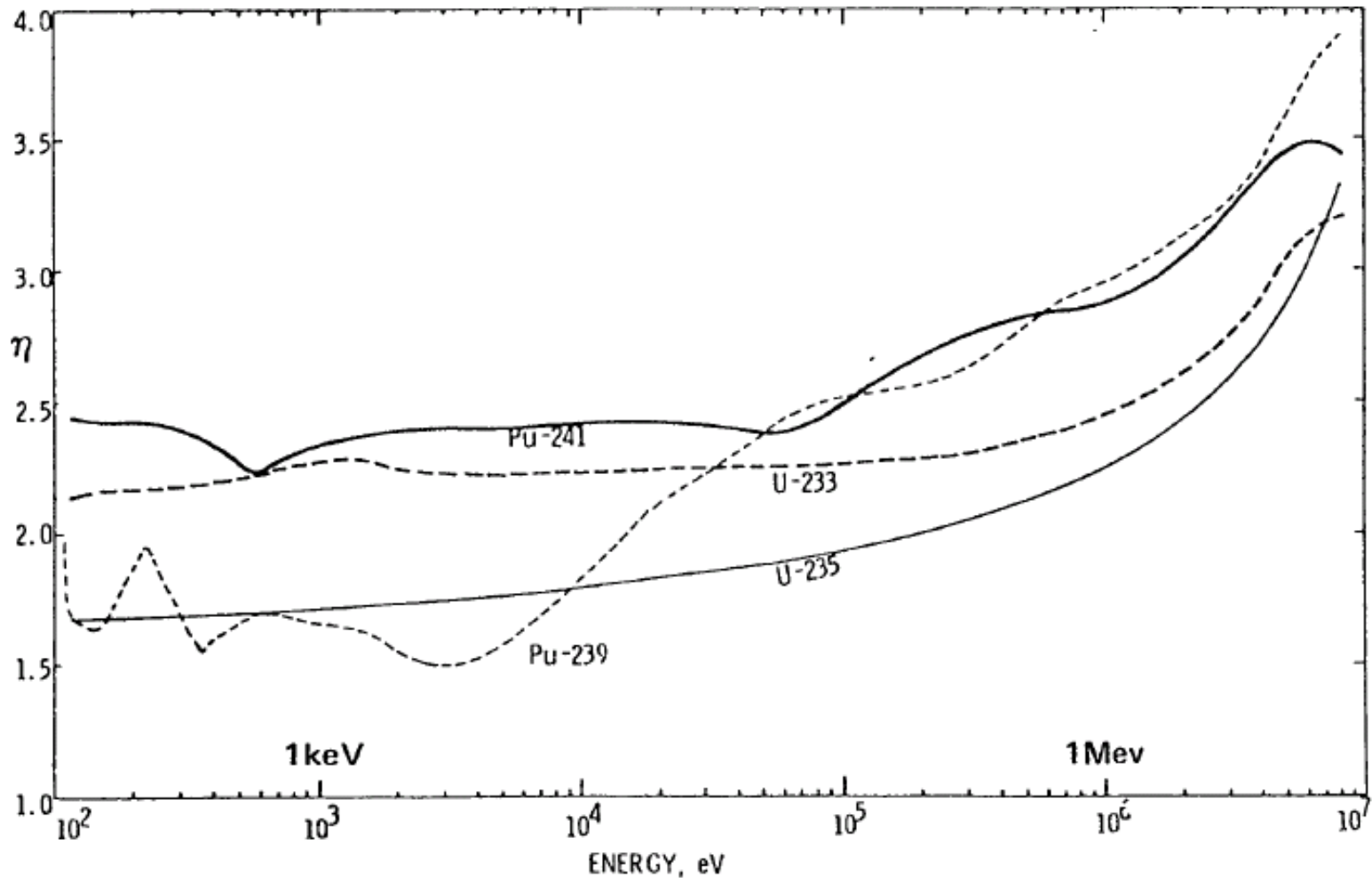
- Depletion Equation
- Definition of burnup
  - thermal energy output per mass of fuel
  - MWD/MTHM

# Transmutation

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- Equation for production of any nuclide
- Conversion versus Breeding
  - Depending on core physics design of the reactor core
  - $\eta$  (eta)
    - Number of neutrons produced/absorbed in fuel
- Conversion ratio
  - rate of creation of new fissile/destruction of existing fissile





**FIGURE 6-1**

Values of eta [ $\eta$ ] for fissile nuclides as a function of energy. [Courtesy of Electric Power Research Institute (Shapiro, 1977).]



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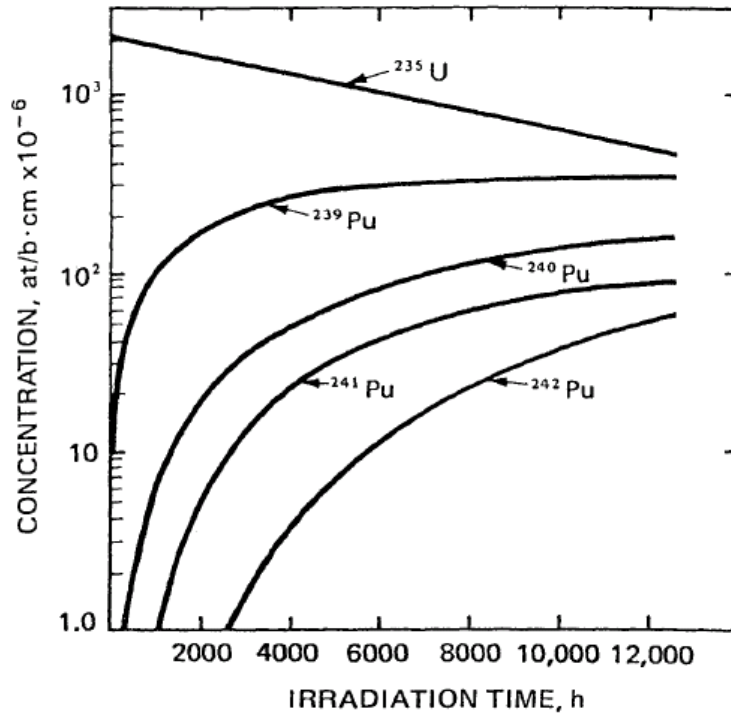
# Breeding Ratios for Reactor Systems

**TABLE 6-1**  
Average Conversion or Breeding Ratios for Reference Reactor Systems

Reference reactor	Initial fuel <sup>†</sup>	Conversion cycle <sup>†</sup>	Conversion ratio	Breeding ratio
BWR	2–4 wt% <sup>235</sup> U	<sup>238</sup> U–Pu	0.6	—
PWR	2–4 wt% <sup>235</sup> U	<sup>238</sup> U–Pu	0.6	—
PTGR	1.8–2.1 wt% <sup>235</sup> U	<sup>238</sup> U–Pu	≥0.6	—
PHWR	Natural U	<sup>238</sup> U–Pu	0.8	—
HTGR	≈5 wt% <sup>235</sup> U	<sup>232</sup> Th– <sup>233</sup> U	0.8	—
LMFBR	10–20 wt% Pu	<sup>238</sup> U–Pu	—	1.0–1.6

<sup>†</sup> All plutonium in power reactors is an isotopic mixture based on initial conversion of <sup>238</sup>U to <sup>239</sup>Pu and followed by transmutation to the “higher” isotopes.

# Buildup of Plutonium with Burnup



<http://atom.kaeri.re.kr/>

**FIGURE 6-2**

Buildup of plutonium isotopes with burnup for a representative LWR fuel composition.



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# Reactivity Penalty

**TABLE 6-2**  
Reactivity Penalty from Selected Transmutation Products  
for Recycle of BWR Fuel<sup>†</sup>

End of cycle number	Reactivity penalty at discharge, % $\Delta k$			
	<sup>236</sup> U <sup>‡</sup>	<sup>237</sup> Np <sup>§</sup>	<sup>242</sup> Pu	<sup>243</sup> Am <sup>§</sup>
1	0.62	0.13	0.65	0.36
2	0.90	0.59	1.53	0.57
3	1.12	0.73	2.04	0.89

<sup>†</sup>From A. Sesonske, *Nuclear Power Plant Design Analysis*, TID-26241, 1973.


<sup>‡</sup>The <sup>236</sup>U concentration is assumed not to decrease in the diffusion plant.

<sup>§</sup>Neptunium and americium are removed by reprocessing on each recycle.



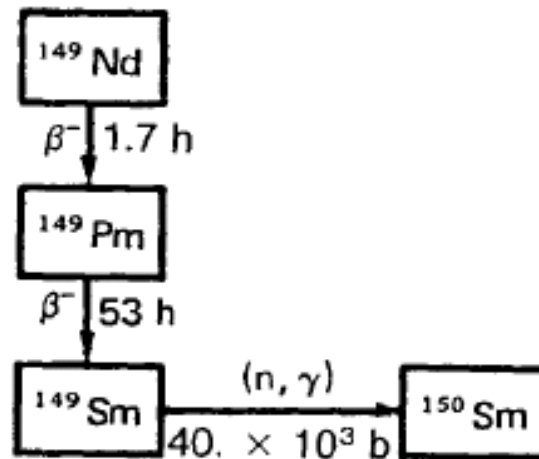
# Fission Products

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- Fission Fragments  Fission Products
  - Rate of Creation -  $\gamma \Sigma_f \Phi$
  - $\gamma$  fission yield
- Fission Fragment Balance Equation

# Samarium Buildup

172 Basic Theory



(a)

FISSILE NUCLIDE	$\gamma^{Nd}$
$^{233}\text{U}$	0.0066
$^{235}\text{U}$	0.0113
$^{239}\text{Pu}$	0.0190

(b)



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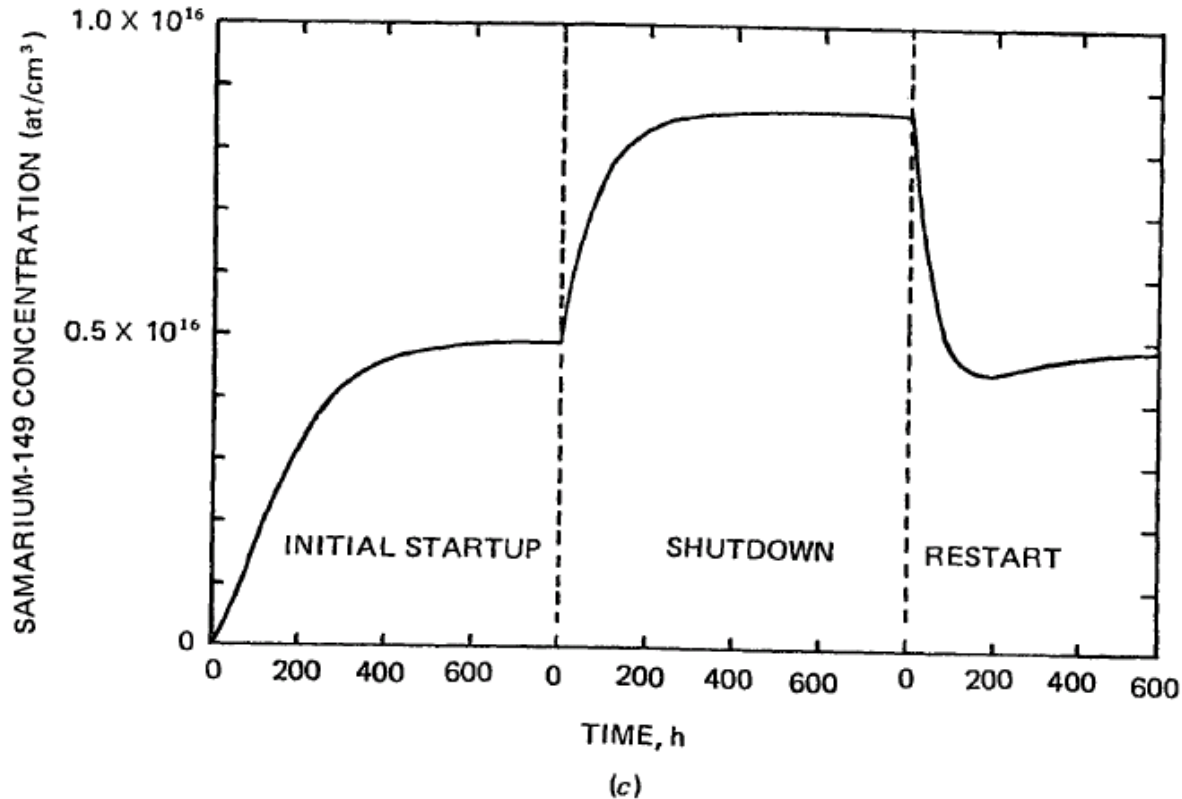
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# Samarium Buildup



**FIGURE 6-6**

Behavior of  $^{149}\text{Sm}$  in representative LWR fuel: (a) decay and reaction chain, (b) fission yields, (c) concentration vs. time.



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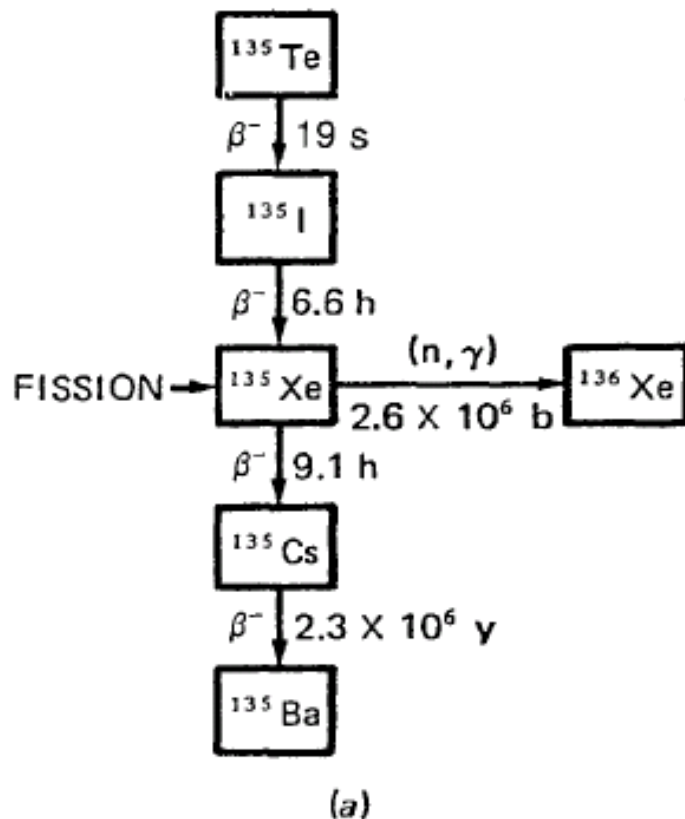
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# Xenon Buildup

174 Basic Theory



FISSILE NUCLIDE	$\gamma(^{135}\text{Te})$	$\gamma(^{135}\text{Xe})$
$^{233}\text{U}$	0.051	0.003
$^{235}\text{U}$	0.061	
$^{239}\text{Pu}$	0.055	

(b)



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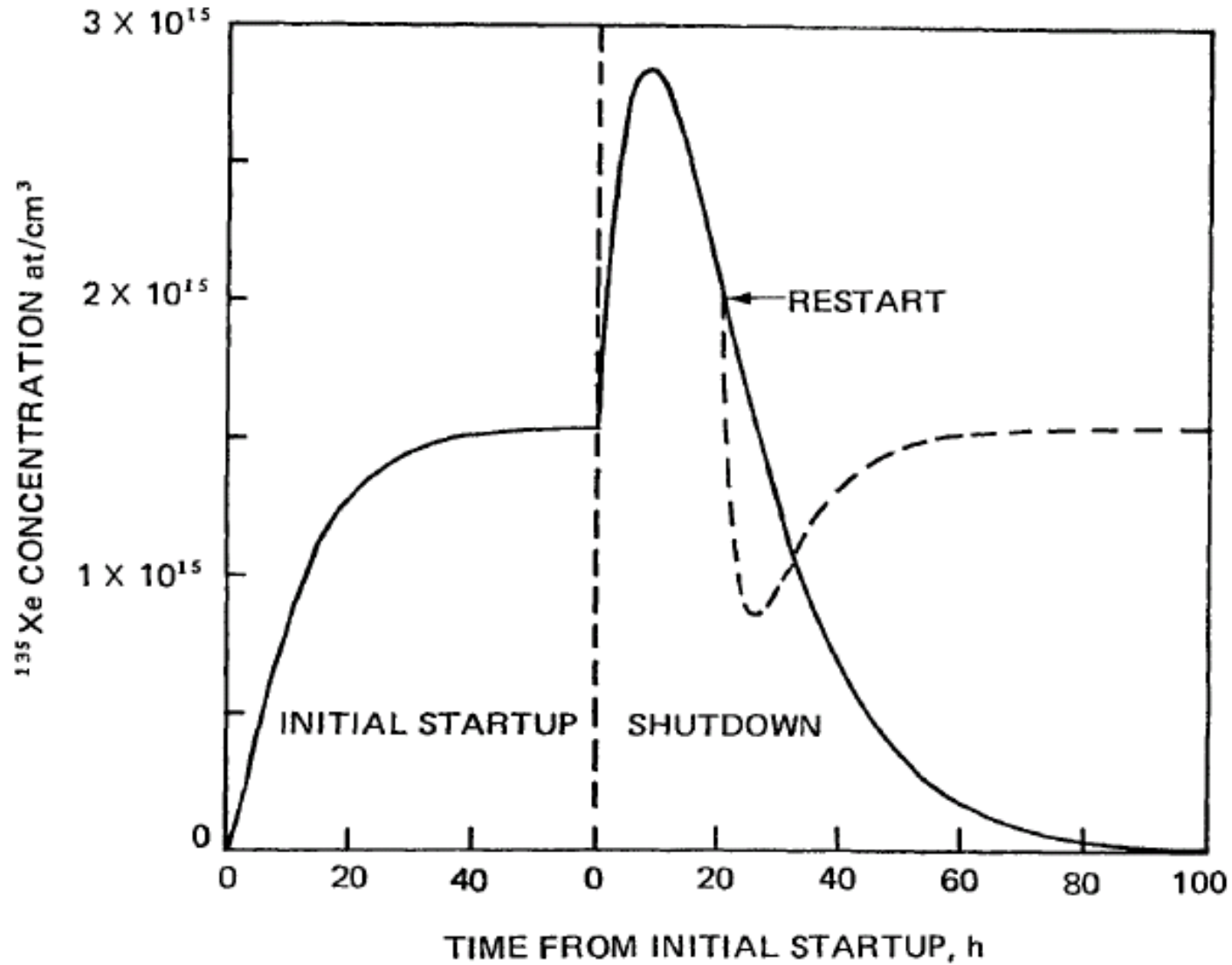
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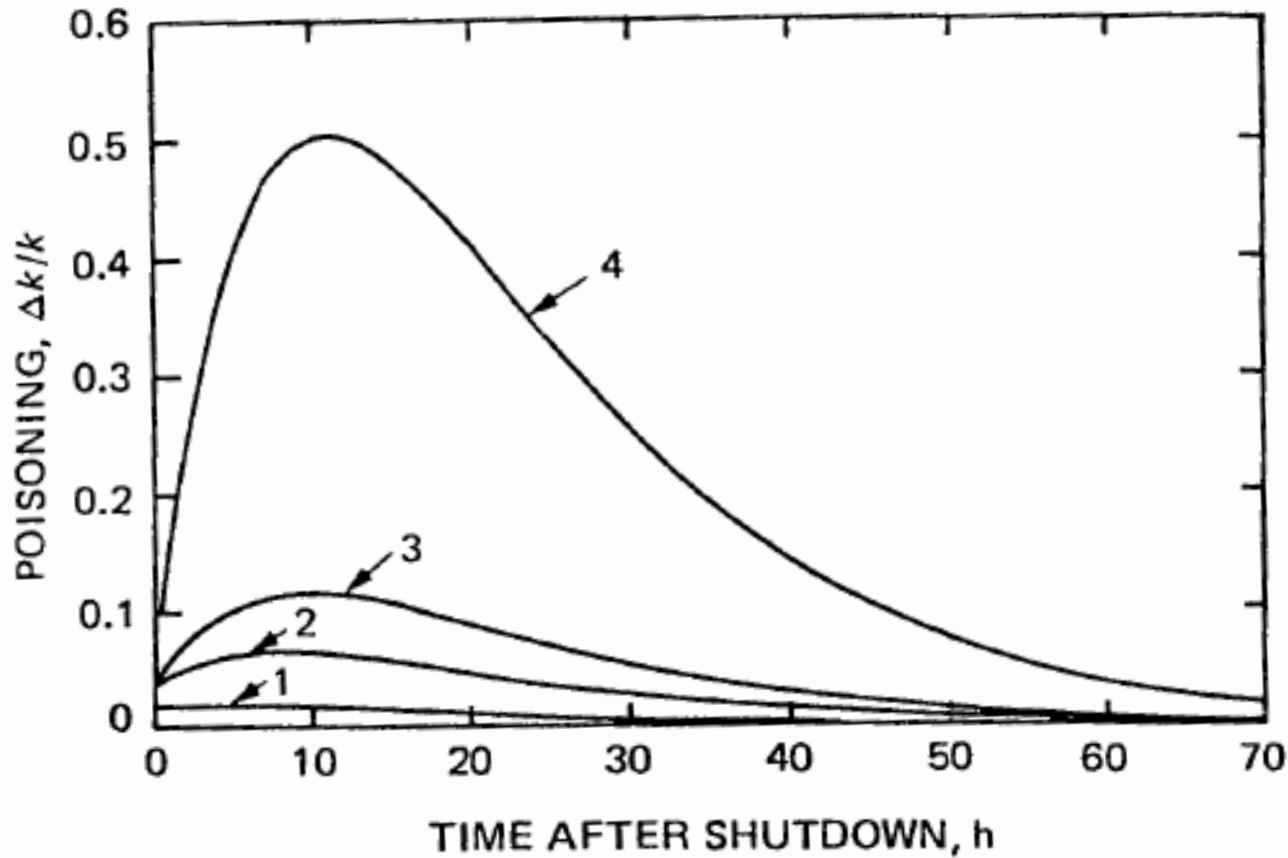
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(c)

**FIGURE 6-7**

Behavior of  $^{135}\text{Xe}$  in representative LWR fuel: (a) decay and reaction chain, (b) fission yields, (c) concentration vs. time.

**FIGURE 6-8**

Poisoning of  $^{135}\text{Xe}$  as a function of time after shutdown for a representative LWR fuel composition at various neutron flux levels. Curve 1:  $\Phi = 1 \times 10^{13} \text{ n/cm}^2\cdot\text{s}$ ; Curve 2:  $\Phi = 5 \times 10^{13} \text{ n/cm}^2\cdot\text{s}$ ; Curve 3:  $\Phi = 1 \times 10^{14} \text{ n/cm}^2\cdot\text{s}$ ; Curve 4:  $\Phi = 5 \times 10^{14} \text{ n/cm}^2\cdot\text{s}$ .

# Operational Impacts

- Xenon Oscillations
- Fuel Design for cycle length of core
- Fuel management strategies
- Power peaking limits
- Power distribution control



# Reactor Physics Calculations

- Multi-Group Diffusion Equations
  - Model core – using fuel pin and assembly homogenization of materials and fuels with pins averaged horizontally but detailed axially
- Run Static calculation for core power and flux distribution
- Fluxes used to perform depletion calculations as noted for a “time step”
- New material calculations used to produce new power and flux distribution for next “time step” – 1 month
- Incorporate only significant isotopes – high absorption and/or fission cross sections ignoring short lived isotopes in decay chains. – use lumping procedure
- Need to consider early xenon and Samarium build up 50 hours/500 hours
- Track key isotopes for all fuel assemblies for refueling management

# Homework Assignment

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- Chapter 6
  - Problems: 6.2, 6, 7, 9, 11, 15

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