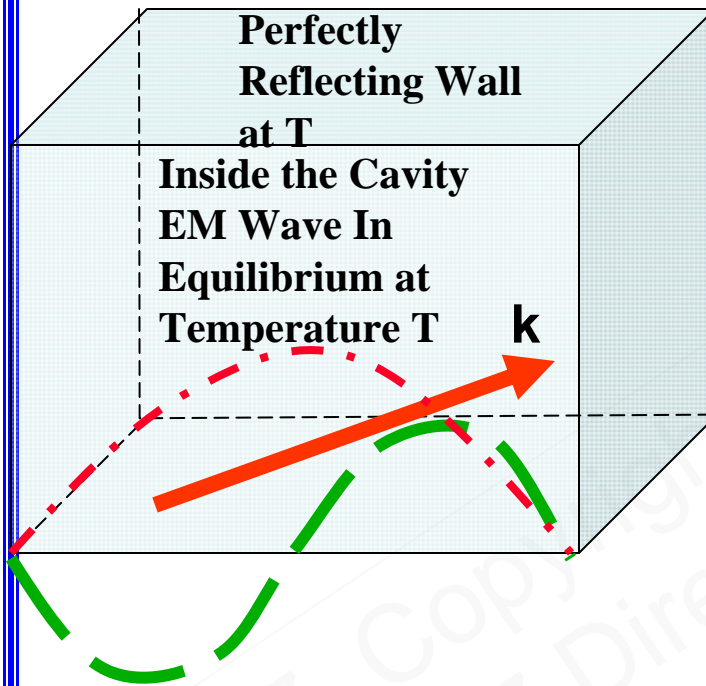


Thermal Radiation: Planck's Law



Basic Relations

Frequency ν

Angular Frequency $\omega = 2\pi\nu$

Wavelength λ

Wavevector magnitude $k = 2\pi/\lambda$

Wavevector $\mathbf{k} = (k_x, k_y, k_z)$

$$c = \nu\lambda \quad \longrightarrow \quad \omega = ck = c\sqrt{k_x^2 + k_y^2 + k_z^2}$$

$\omega(\mathbf{k})$: Dispersion relation (linear)

How much energy in the cavity?

$$L_x = \frac{\lambda_x}{2}, 2\frac{\lambda_x}{2}, \dots, n_x \frac{\lambda_x}{2}, \dots$$

$$k_x = n_x \frac{2\pi}{2L_x}$$

Two polarization

$$U = 2 \sum_{n_x=1}^{\infty} \sum_{n_y=1}^{\infty} \sum_{n_z=1}^{\infty} \hbar\omega f(\omega, T) =$$

$$2 \int_0^{\infty} \frac{dk_x}{(2\pi/2L_x)} \int_0^{\infty} \frac{dk_y}{(2\pi/2L_y)} \int_0^{\infty} \frac{dk_z}{(2\pi/2L_z)} \hbar\omega f(\omega, T)$$

$$= 2 \int_{-\infty}^{\infty} \frac{dk_x}{(2\pi/L_x)} \int_{-\infty}^{\infty} \frac{dk_y}{(2\pi/L_y)} \int_{-\infty}^{\infty} \frac{dk_z}{(2\pi/L_z)} \hbar\omega f(\omega, T)$$

Thermal Radiation: Planck's Law

$$U = \frac{2V}{8\pi^3} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \hbar \omega f(\omega, T) dk_x dk_y dk_z$$

$$= \frac{2V}{8\pi^3} \int_0^{\infty} \hbar \omega f(\omega, T) 4\pi k^2 dk$$

$$= \frac{2V}{8\pi^3} \int_0^{\infty} \hbar \omega f(\omega, T) 4\pi \left(\frac{\omega}{c}\right)^2 d\left(\frac{\omega}{c}\right)$$

$$\frac{U}{V} = \int_0^{\infty} \hbar \omega f(\omega, T) \frac{\omega^2}{\pi^2 c^3} d\omega$$

$$= \int_0^{\infty} \hbar \omega f(\omega, T) D(\omega) d\omega$$

$$= \int_0^{\infty} u(\omega) d\omega$$

D(ω)-density of states per unit volume per unit angular frequency interval

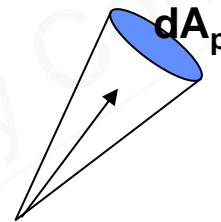
- **Energy density per ω interval**

$$u(\omega) = \hbar \omega f(\omega, T) D(\omega)$$

$$= \frac{\hbar \omega^3}{\pi^2 c^3} \frac{1}{\exp\left(\frac{\hbar \omega}{k_B T}\right) - 1}$$

Planck's law

- **Intensity: energy flux per unit solid angle**



Solid Angle

$$d\Omega = \frac{dA_p}{R^2}$$

whole space
4π

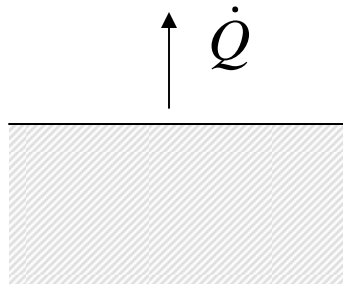
$$I(\omega) = \frac{cu(\omega)}{4\pi} = \frac{\hbar \omega^3}{4\pi^3 c^2} \frac{1}{\exp\left(\frac{\hbar \omega}{k_B T}\right) - 1}$$

Per unit wavelength interval

$$I(\lambda) = \left| \frac{I(\omega) d\omega}{d\lambda} \right| = \frac{4\pi \hbar c}{\lambda^5} \frac{1}{\exp\left(\frac{2\pi \hbar c}{k_B T \lambda}\right) - 1}$$

Planck's law

Thermal Radiation: Planck's Law



Wien's displacement law

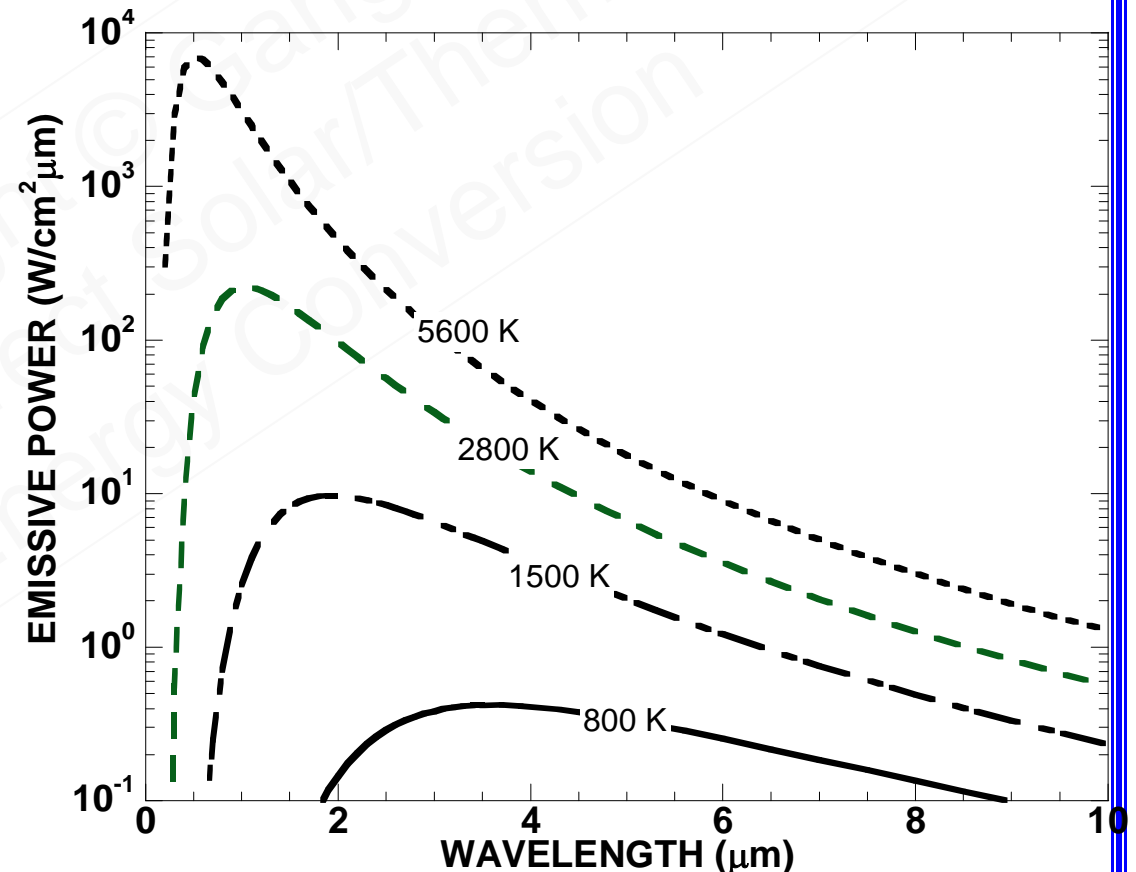
$$\lambda_{\max} T = 2898 \text{ K}\mu\text{m}$$

Emissive Power

$$\begin{aligned} \dot{Q}(\lambda) &= A\pi I(\lambda) \\ &= A \frac{\hbar\omega^3}{4\pi^2 c^2} \frac{1}{\exp\left(\frac{\hbar\omega}{k_B T}\right) - 1} \end{aligned}$$

Total

$$\dot{Q} = \int_0^{\infty} \dot{Q}(\lambda) d\lambda = A\sigma T^4$$



Introduction to Thermoelectricity

Gang Chen

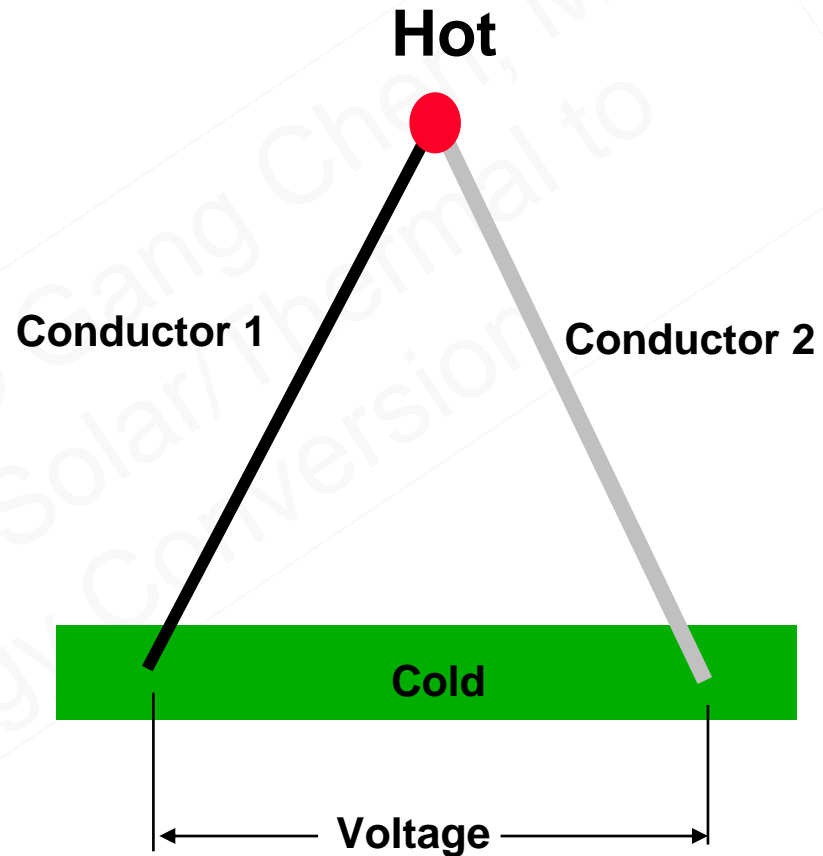
**Mechanical Engineering Department
Massachusetts Institute of Technology**

URL: <http://web.mit.edu/nanoengineering>

Seebeck Effect



Thomas Johann Seebeck
1770-1831



Seebeck effect: Discovered in 1821
Temperature difference generates voltage

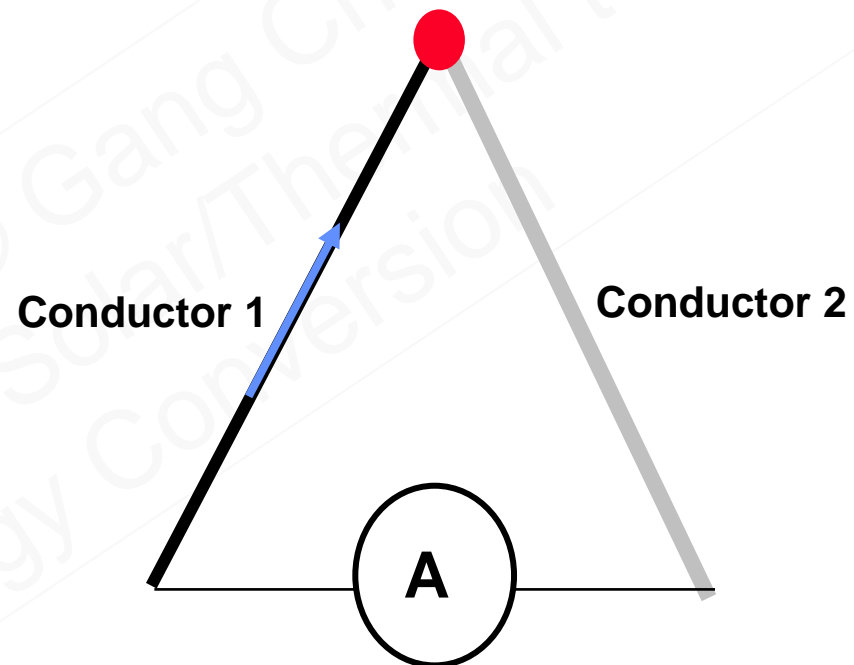
<http://www.sil.si.edu/silpublications/dibner-library-lectures/scientific-discoveries/text-lecture.htm>

Peltier Effect



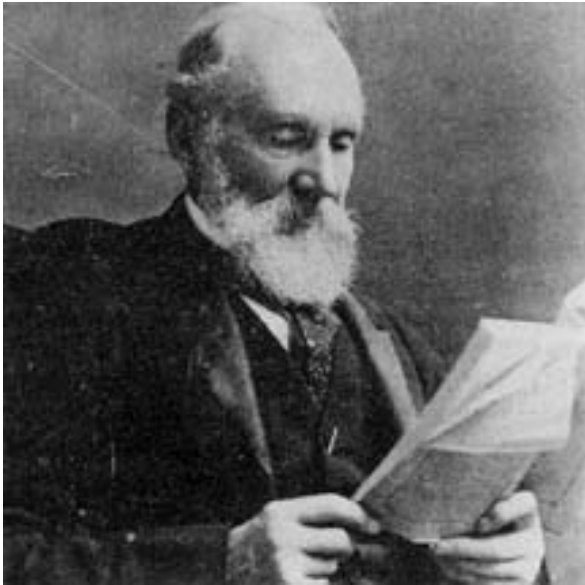
Jean Charles Athanase Peltier
1785-1845

Heating or Cooling



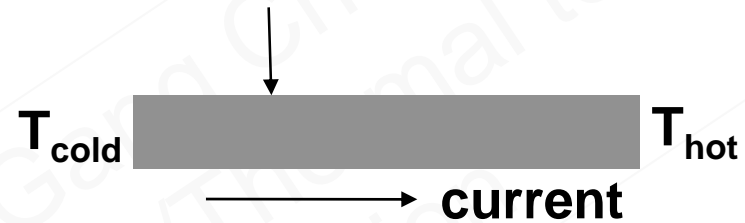
Peltier Effect: Discovered in 1834
An electrical current creates a cooling or heating effect at the junction depending on the direction of current flow.

Thomson Effect



**William Thomson
(Lord Kelvin)
1824 – 1907**

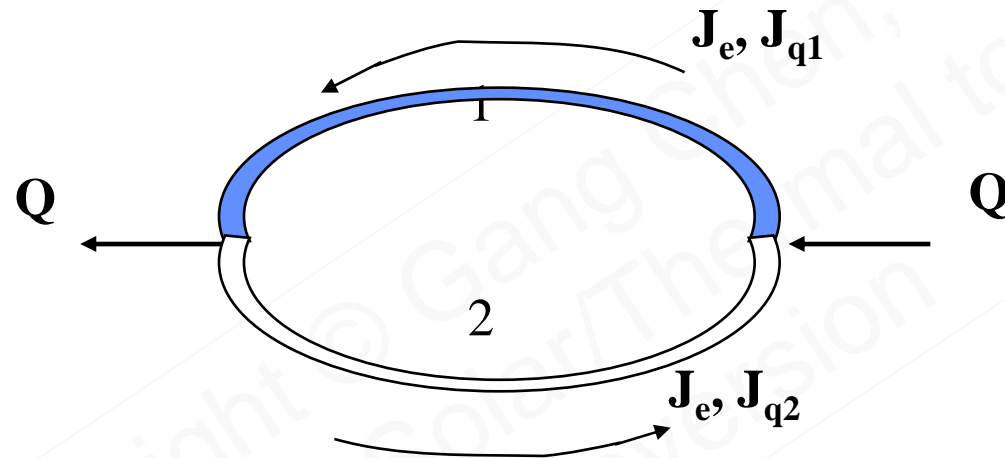
heat release/absorption $q(x)$



Thomson effect predicted, 1855

<http://www.sil.si.edu/silpublications/dibner-library-lectures/scientific-discoveries/text-lecture.htm>

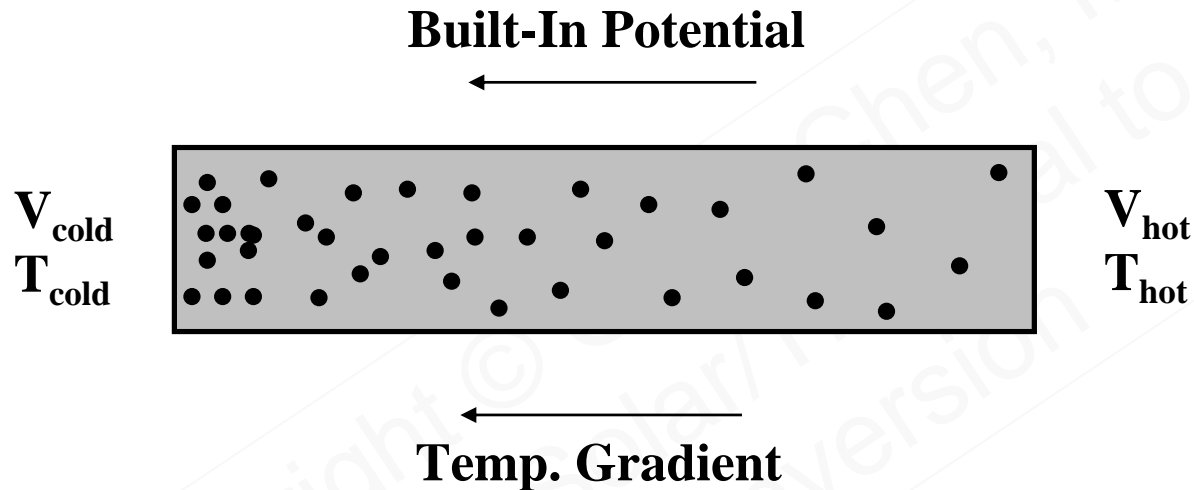
Peltier Effect



$$Q \text{ (Peltier)} = (\Pi_1 - \Pi_2)J$$

- Heating and cooling at junctions
- Reversible with current direction

Seebeck Effect

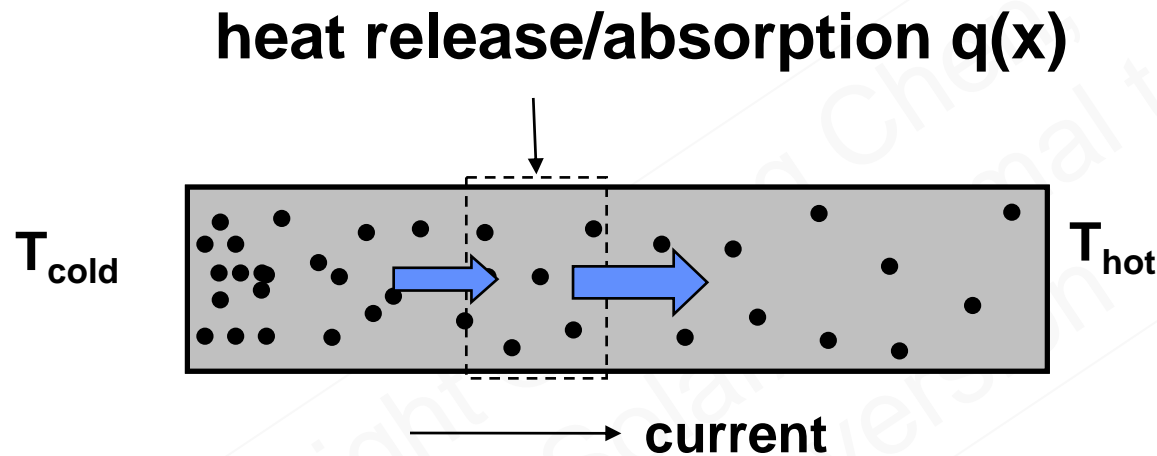


- Charge diffusion under a temperature gradient
- Built-in potential resisting diffusion

$$S = -\Delta V / \Delta T = -(V_{\text{hot}} - V_{\text{cold}}) / (T_{\text{hot}} - T_{\text{cold}})$$

S --- Seebeck Coefficient

Thomson Effect



Thomson Coefficient

$$\tau = \frac{1}{I} \frac{dq}{dx} \bigg/ \frac{dT}{dx}$$

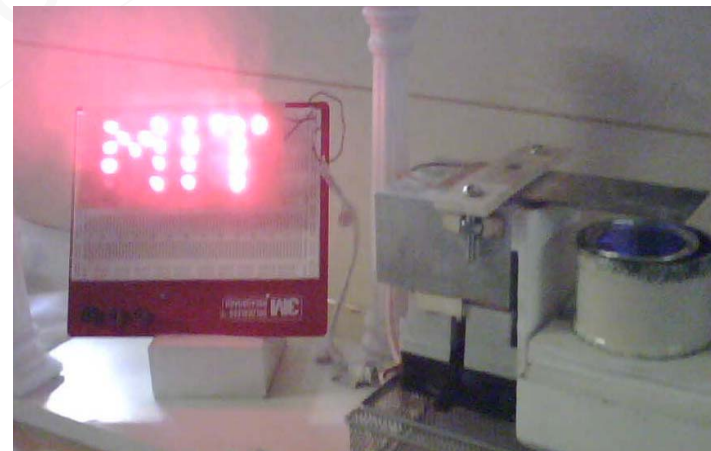
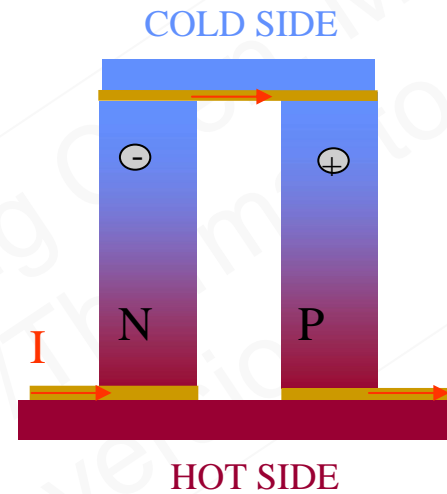
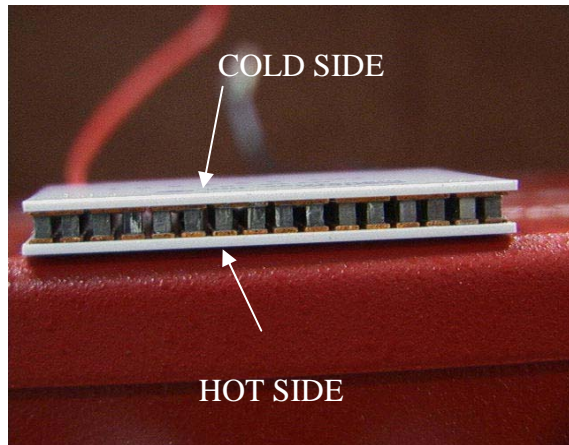
- **Kelvin Relations:** $\Pi = ST$; $\tau = T dS/dT$

Properties are Temperature Dependent

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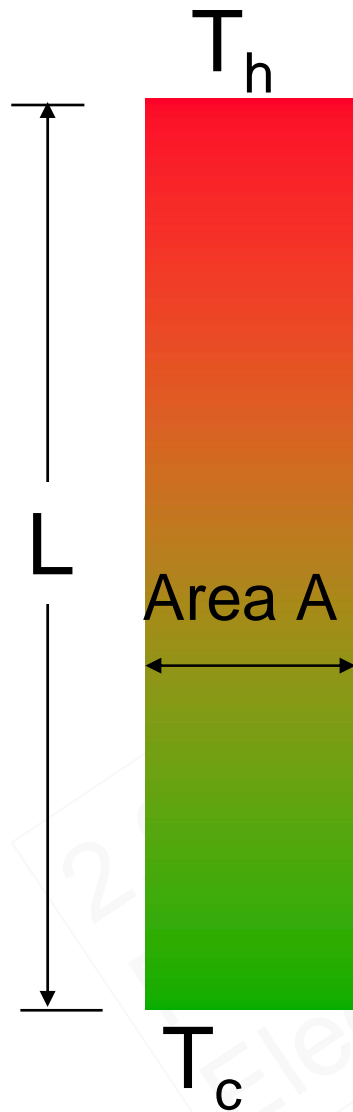
Please see Fig. 2a,b in Poudel, Bed, et al. "High-Thermoelectric Performance of Nanostructured Bismuth Antimony Telluride Bulk Alloys." *Science* 320 (May 2, 2008): 634-638.

Thermoelectric Devices



Performance of Thermoelectric Devices

Other Basic Relations: Heat Conduction



- Fourier Law for heat conduction

$$\mathbf{q} = -k \nabla T$$

Heat Flux [W/m^2]

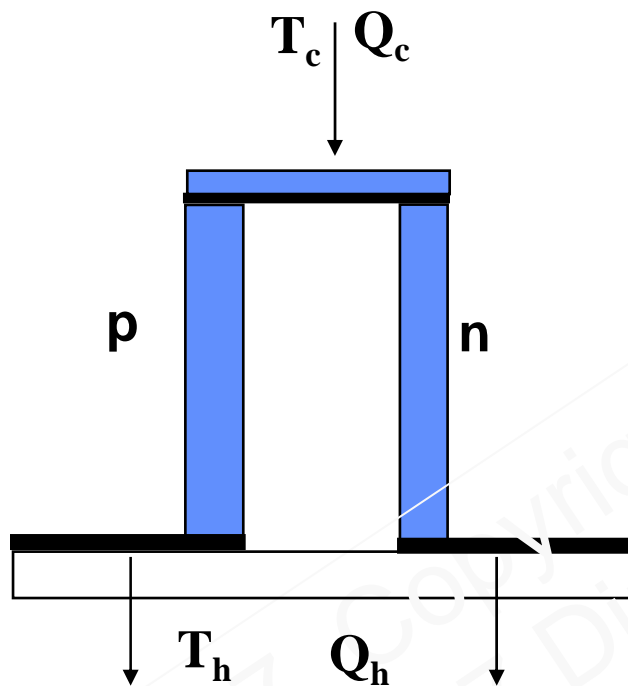
Thermal Conductivity [$\text{W}/\text{m}\cdot\text{K}$]

- One-dimensional heat conduction

$$Q = Ak \frac{T_h - T_c}{L} = K \Delta T$$

$$\text{Thermal Conductance : } K = \frac{kA}{L}$$

Device Analysis: Cooling



- **Ideal Devices**

**No Joule Heating,
No Heat Conduction**

$$Q_c = (\Pi_p - \Pi_n) \cdot I$$

- **Real Devices:**

Joule Heating & Heat Conduction

$$Q_c = (\Pi_p - \Pi_n) \cdot I - I^2 R / 2 - K (T_h - T_c)$$

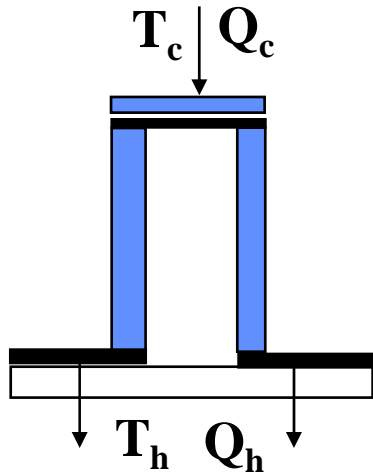
Electrical Resistance

Thermal Conductance

$$R = \frac{L_p \rho_p}{A_p} + \frac{L_n \rho_n}{A_n}$$

$$K = \frac{k_p A_p}{L_p} + \frac{k_n A_n}{L_n}$$

Refrigerator Performance



Voltage Drop: $V = IR + (S_p - S_n)(T_h - T_c)$

Coefficient of Performance:

$$\phi = \frac{Q_C}{W} = \frac{(S_p - S_n)IT_C - K(T_H - T_C) - \frac{1}{2}I^2R}{(S_p - S_n)I(T_H - T_C) + I^2R}$$

Optimize Current:

$$\phi_{\max} = \frac{T_C}{(T_H - T_C)} \frac{\sqrt{1 + ZT_M} - \frac{T_H}{T_C}}{\sqrt{1 + ZT_M} + 1}$$

$$\uparrow T_M = 0.5(T_h + T_c)$$

$$Z = \frac{(S_p - S_n)^2}{KR} = \frac{(S_p - S_n)^2}{\left(\frac{L_p \rho_p}{A_p} + \frac{L_n \rho_n}{A_n}\right) \left(\frac{k_p A_p}{L_p} + \frac{k_n A_n}{L_n}\right)}$$

Figure of Merit Z

$$KR = \left(\frac{L_p \rho_p}{A_p} + \frac{L_n \rho_n}{A_n} \right) \left(\frac{k_p A_p}{L_p} + \frac{k_n A_n}{L_n} \right)$$

$$(KR)_{\min} = \left(\sqrt{k_p \rho_p} + \sqrt{k_n \rho_n} \right)^2 \quad \text{when} \quad \frac{L_n A_p}{L_p A_n} = \left(\frac{\rho_p k_n}{\rho_n k_p} \right)^{1/2}$$

$$Z_{\max} = \frac{(S_p - S_n)^2}{\left(\sqrt{k_p \rho_p} + \sqrt{k_n \rho_n} \right)^2} \quad \text{For a single material:} \quad Z = \frac{S^2}{\rho k} = \frac{\sigma S^2}{k}$$

In a device, pn pairs are used:

- (1) Areas of each type of legs need to be optimized
- (2) Two types of legs should have comparable properties
- (3) Current input to the device needs to be optimized

Typical Number

- Bi_2Te_3 -based materials ~ 300 K

$$\begin{aligned} S &= 220 \mu\text{V/K} \\ \sigma &= 10^5 \text{ Sm}^{-1} \\ k &= 1.5 \text{ W/mK} \end{aligned}$$

$$\begin{aligned} \text{Power Factor: } S^2\sigma &= 48 \mu\text{W/cm-K} \\ \text{Figure of Merit: } Z &= 3.2 \times 10^{-3} \text{ 1/K} \\ ZT &= 1 \end{aligned}$$

- Device Leg: 1 mm x 1 mm x 2 mm

$$R_1 = \frac{L}{\sigma A} = \frac{2 \times 10^{-3}}{10^5 \times 10^{-6}} = 0.02 \quad \Omega$$

Legs are electrically in series
but thermally in parallel

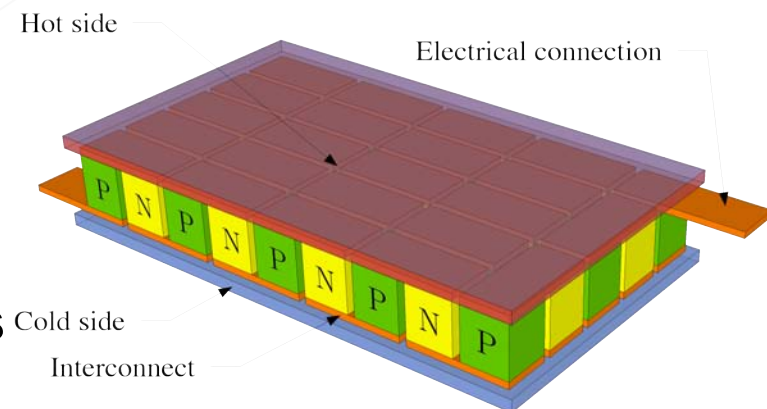
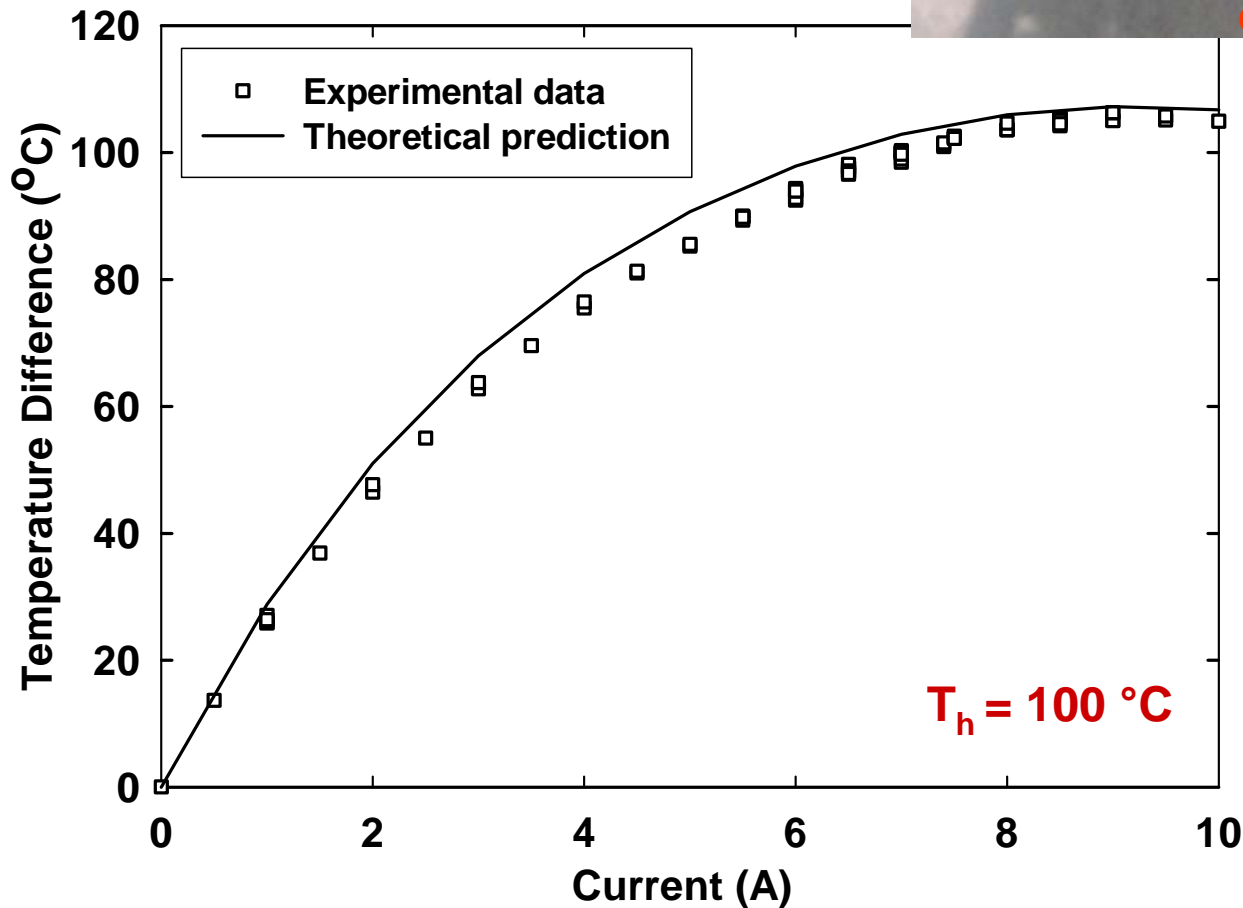
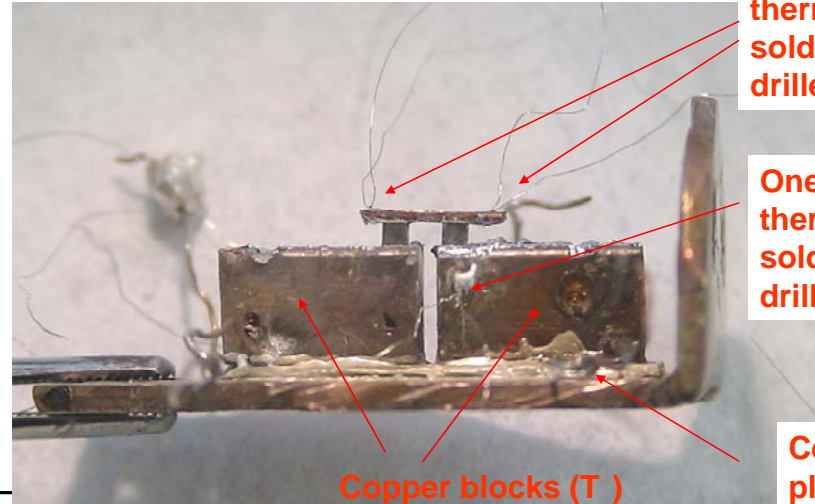


Image by michbich at Wikipedia.

An Example

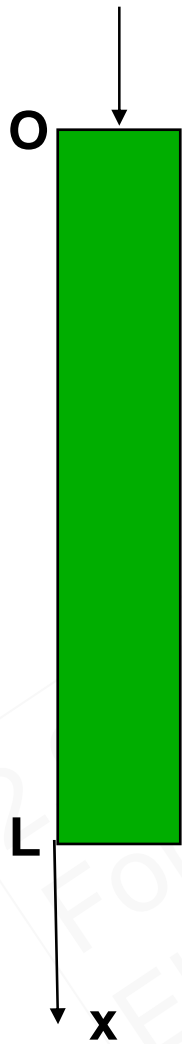


- Match two leg size
- Minimize contact resistance
- Optimize current

Temperature Dependence of Properties

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Please see Fig. 2a,b,d,e in Poudel, Bed, et al.
"High-Thermoelectric Performance of Nanostructured
Bismuth Antimony Telluride Bulk Alloys." *Science* 320 (May 2, 2008): 634-638.

Differential Analysis



$$\frac{d}{dx^2} \left(k \frac{dT}{dx} \right) - JT \frac{dS}{dT} \frac{dT}{dx} + J^2 \rho = 0$$

Thomson Effect, Usually Neglected

Joule Heating

Boundary Conditions (Cooling):

$$x=0: \quad T_c \text{ given or } q_c = -k \frac{dT}{dx} + \Pi J = -k \frac{dT}{dx} + ST_c J$$

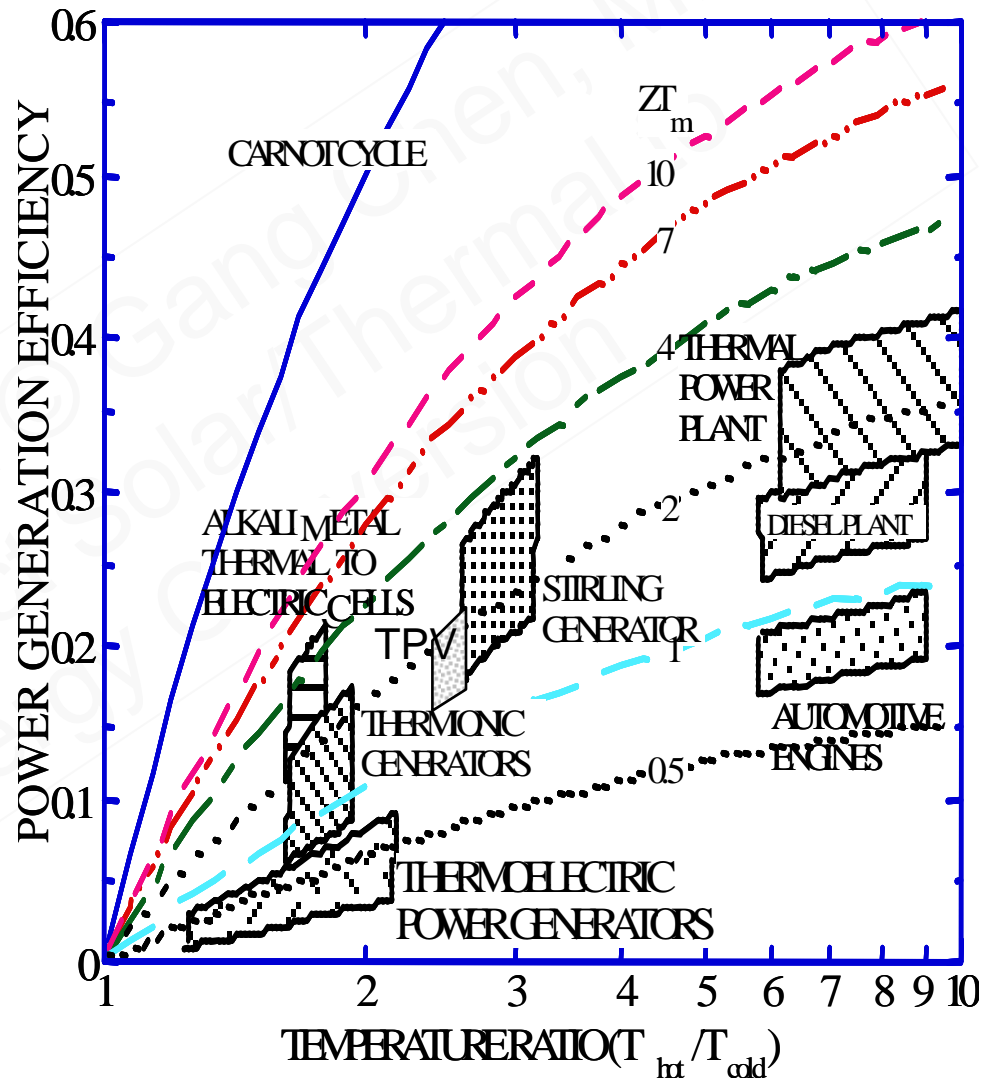
Thermoelectric Power Generation

Efficiency

$$\eta = \left(1 - \frac{T_c}{T_h}\right) \frac{\sqrt{1 + ZT_{ave}} - 1}{\sqrt{1 + ZT_{ave}} + \frac{T_c}{T_h}}$$

$$T_{ave} = \frac{T_c + T_h}{2}$$

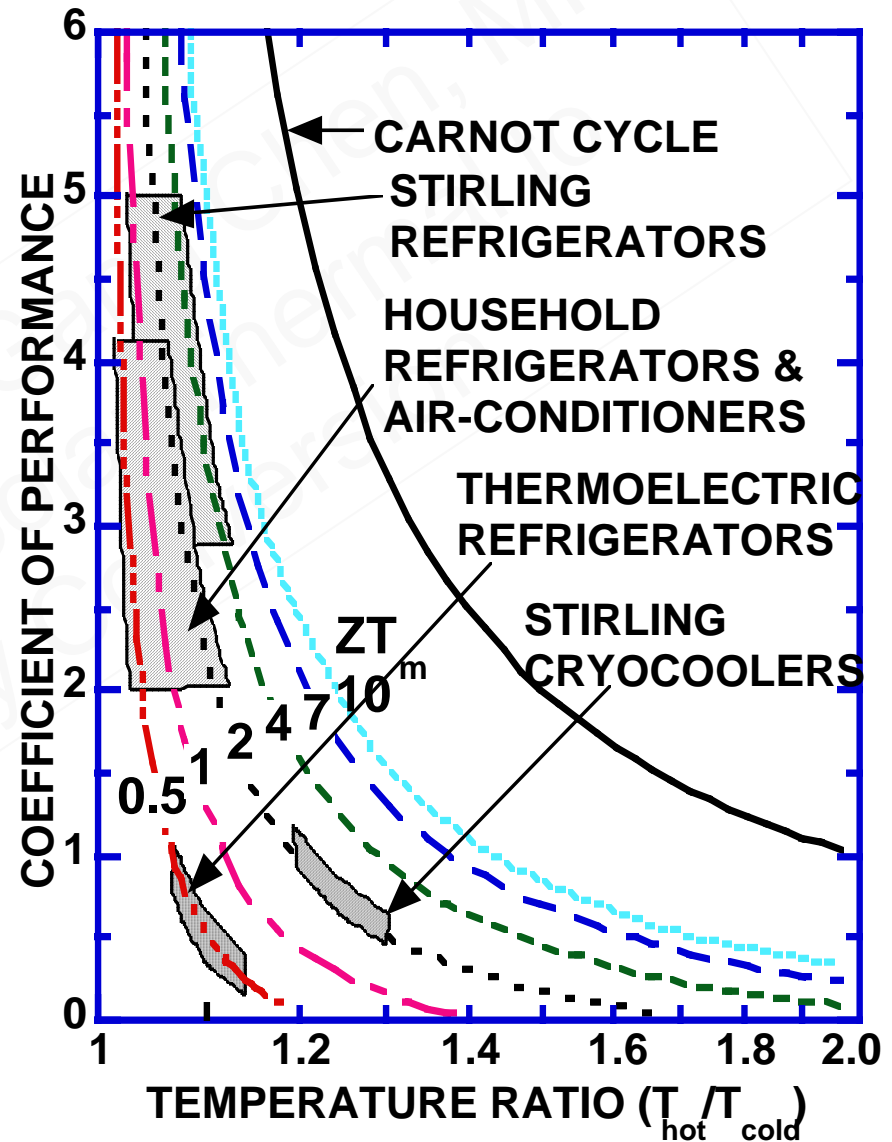
Constant Properties



Thermoelectric Refrigeration

Coefficient of Performance

$$COP = \frac{T_c}{T_h - T_c} \frac{\sqrt{1 + ZT_{ave}} - T_h / T_c}{\sqrt{1 + ZT_{ave}} + 1}$$



Current and Potential Applications

Commercial Thermoelectric Devices

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Please see <http://www.hi-z.com/index.php>
<http://www.marlow.com/thermoelectric-modules/>

Power Generators from Hi-Z

Coolers from Marlow Industries

Current Applications in Refrigeration

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Please see: <http://www.roadtrucker.com/12-volt-coolers-accessories/12-volt-coolers-products/igloo-40-quart-kool-mate-40-12-volt-thermo-electric-cooler-6402.jpg>

<http://image.made-in-china.com/2f0j00kvZEKWVPgtlu/Refrigerator-BC-65A-.jpg>

<http://www.newdavincis.com/images/wc-1682%2016%20bottles.jpg>

<http://www.rmtltd.ru/datasheets/TO812.4MD04116xx.pdf>

http://www.medsystechnology.com/images/gem4000_w32a.jpg

http://amerigon.com/ccs_works.php

Current Applications in Power Generation

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<http://thermoelectrics.caltech.edu/images/mhw-rtg.gif>

http://globalte.com/pdf/teg_5120_spec.pdf

<http://www.roachman.com/thermic/thermic1.jpg>

http://www.research.philips.com/newscenter/pictures/downloads/misc-sustainability_05-0_h.jpg

System Consideration

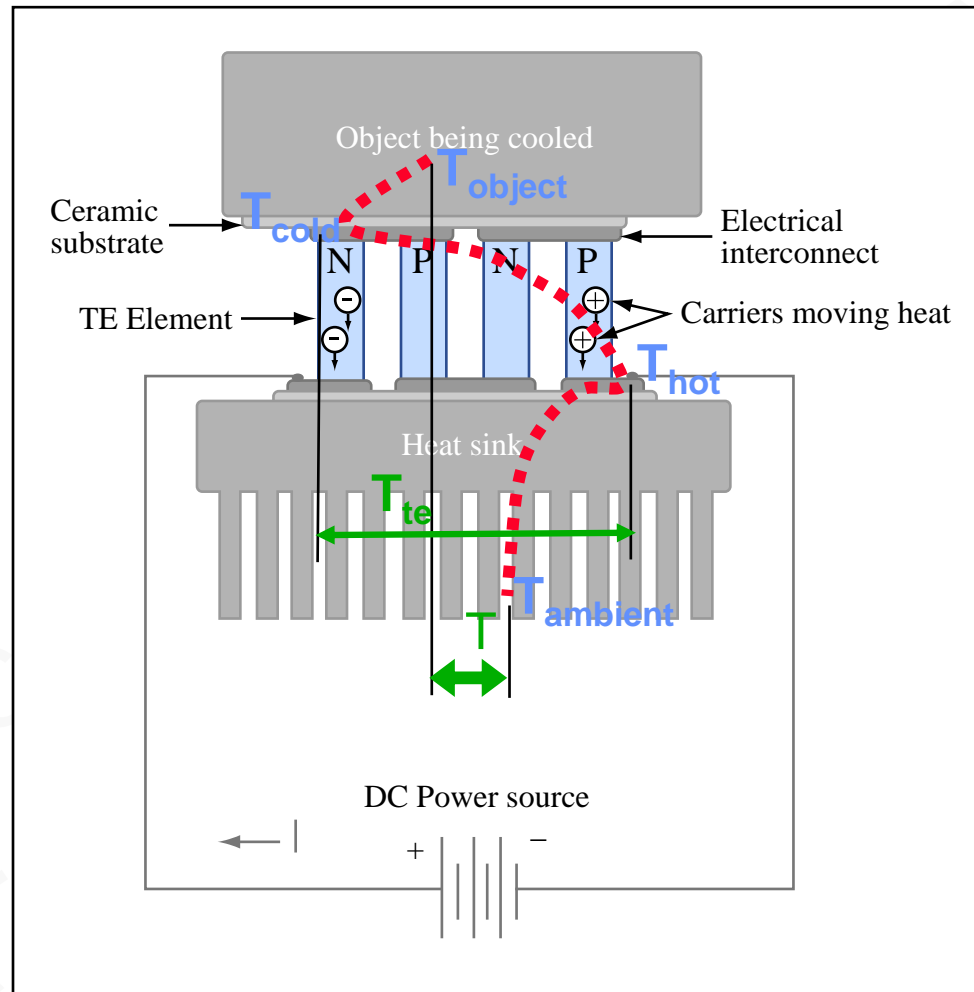
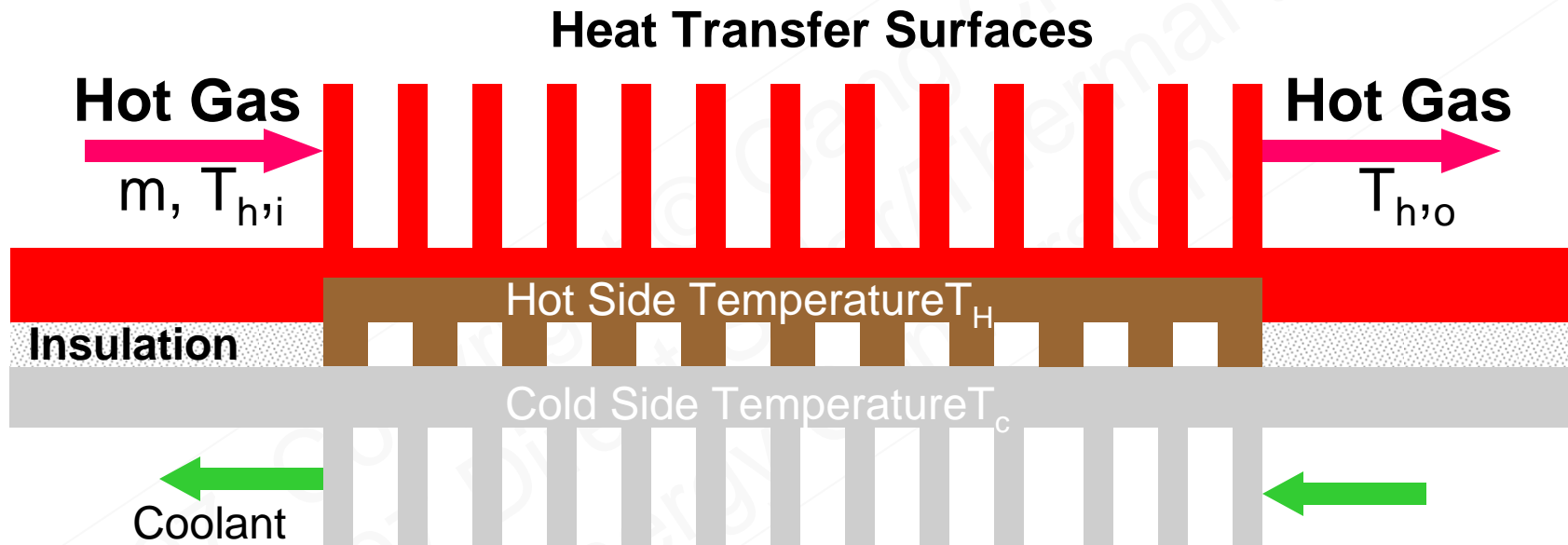


Figure by MIT OpenCourseWare.

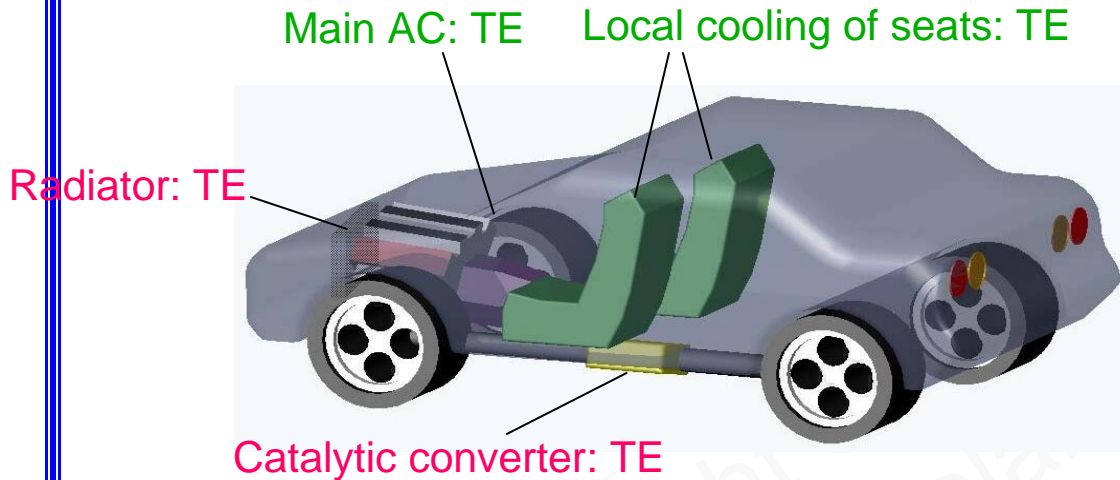
Sometimes, thermal systems more expansive

Heat to Electricity Recovery from Gas Stream

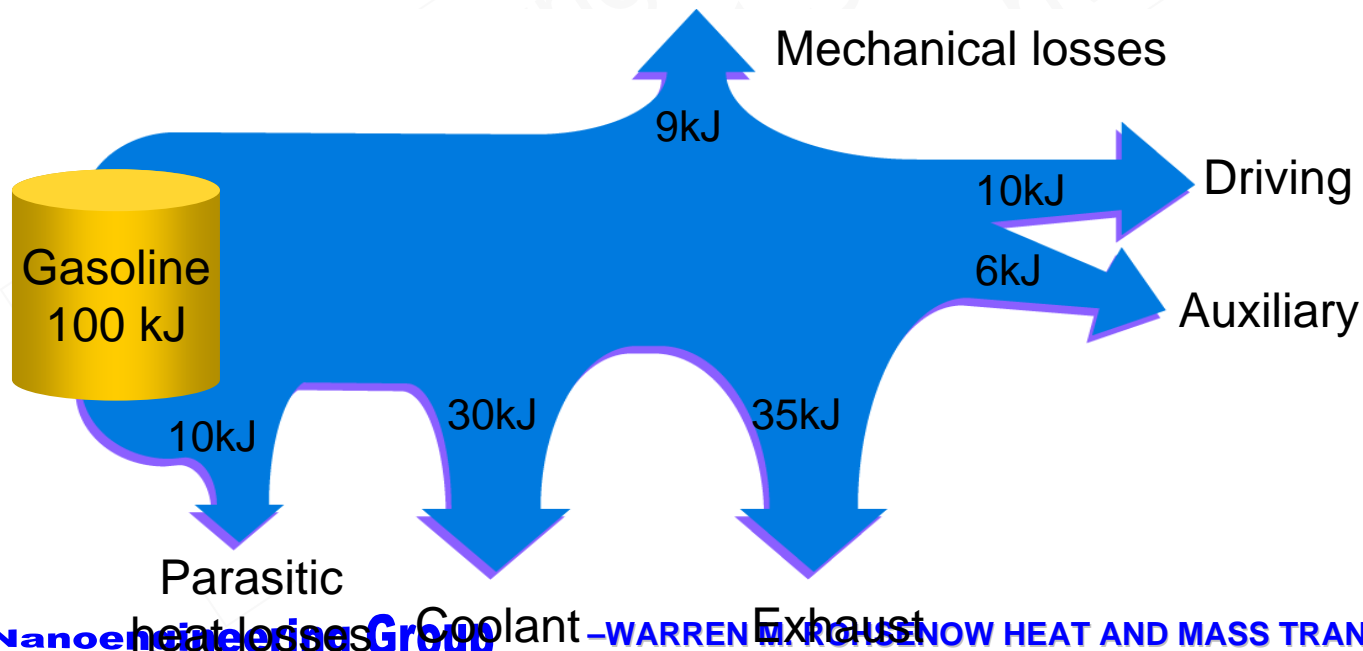


- For thermoelectric devices, T_H higher is better
- However, maximum heat intercepted from hot gas stream, $mc_p(T_{h,i}-T_H)$, decreases with T_H

Vehicle Systems



In US, transportation uses ~26% of total energy.



Prototypes

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<http://cdn-www.greencar.com/images/waste-exhaust-heat-generates-electricity-cars-efficient.php/bmw-teg-1.jpg>

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