



# 13.811

# Advanced Structural Dynamics and Acoustics

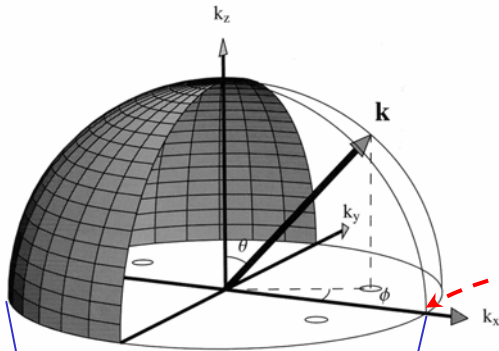
Acoustics  
Lecture 5



# Ewald Sphere Construction Baffled Piston

## Directivity Function

$$D(\theta, \phi) = -\frac{i\rho\omega}{2\pi} \dot{w}_\omega(k_x, k_y; 0)$$

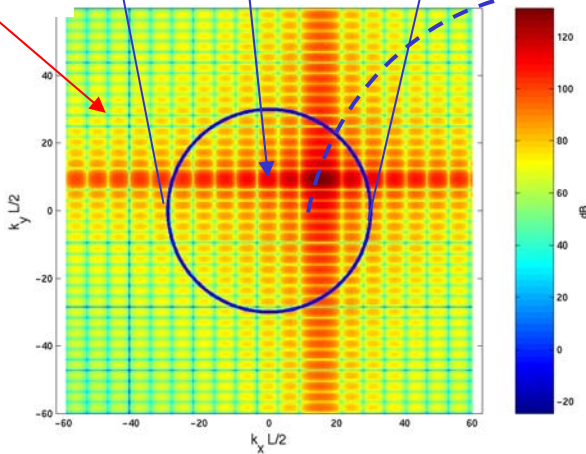


$$f = \omega/2\pi = kc/2\pi$$

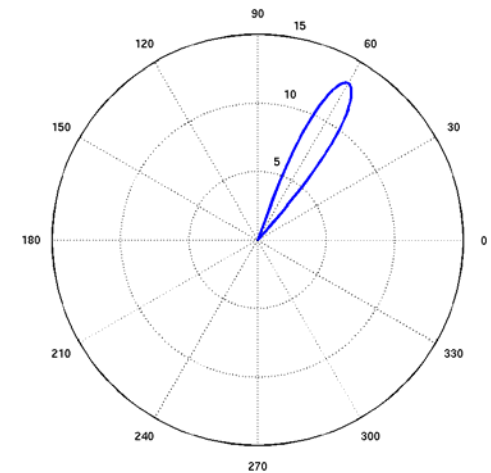
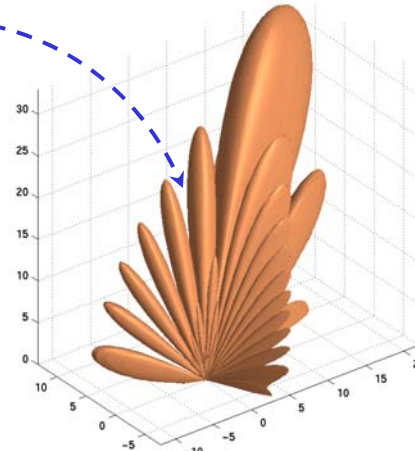
$$k_x = k \sin \theta \cos \phi$$

$$k_y = k \sin \theta \sin \phi$$

Radiating Spectrum  
Evanescent Spectrum



$$kL/2 = 30 - L_x', L_y' = 2, 4 - k_{x0}/k = 0.5$$





# circ.m

```
%
% MATLAB script for plotting the directivity function for
% a circular, baffled piston
%
% Parameters:
% k      Wavenumber
% rho    Density
% c      Speed of Sound
% a      Radius of piston of piston
%
clear
figure(1)
hold off
k=10;
rho=1000;
c=1500;

a=1.0;

ka=k*a;

figure(1);
kxm=2*ka;
nkx=300;
dkx=2*kxm/(nkx-1);
x=[-kxm:dkx:kxm];
y=x;
o=ones(1,nkx);
kx=x' * o;
ky=(y' * o)';
kr=abs(complex(kx,ky));
ss=rho*k*c*a^2 * besselj(1,kr)./kr;
%surf(kx,ky,dba(ss));
wavei(dba(ss)',x,y)
shading('flat')
axis('equal')
b=xlabel('k_x a')
set(b,'FontSize',16);
b=ylabel('k_y a')
set(b,'FontSize',16);
tit=['Circular Piston - ka = ' num2str(k*a) ]
b=title(tit);
set(b,'FontSize',20);
nphi=361;
dphi=2*pi/(nphi-1);
phi=[0:dphi:2*pi];
xx=k*a*cos(phi);
yy=k*a*sin(phi);
hold on
b=plot(xx,yy,'b');
set(b,'LineWidth',3);

figure(2)
nphi=361.
dphi=2*pi/(nphi-1)
nth=181;
dth=0.5*pi/(nth-0.5);

phi=[0:dphi:(nphi-1)*dphi]' * ones(1,nth);
th=( [dth/2:dth:pi/2]' * ones(1,nphi))';
kx=ka*sin(th).*cos(phi);
ky=ka*sin(th).*sin(phi);
kr=ka*sin(th);
ss=rho*k*c*a^2*besselj(1,kr)./kr;

ss=dba(ss);
sm=max(max(ss));
for i=1:size(ss,1)
    for j=1:size(ss,2)
        ss(i,j)=max(ss(i,j),sm-40.0)-(sm-40.0);
    end
end

xx=ss.*sin(th).*cos(phi);
yy=ss.*sin(th).*sin(phi);
zz=ss.*cos(th);

surf(xx,yy,zz);
colormap('copper');
shading('flat');
axis('equal');
tit=['Circular Piston - ka = ' num2str(k*a) ]
b=title(tit);
set(b,'FontSize',20);

figure(3)
b=polar([pi/2-fliplr(th(1,:)) pi/2+th((nphi-1)/2+1,:)],[fliplr(ss(1,:))
ss((nphi-1)/2+1,:)]);
set(b,'LineWidth',2)

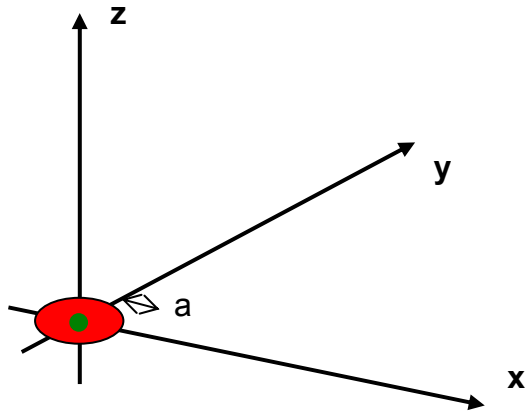
tit=['Circular Piston - ka = ' num2str(k*a) ]
b=title(tit);
set(b,'FontSize',20);
```



# Circular Piston

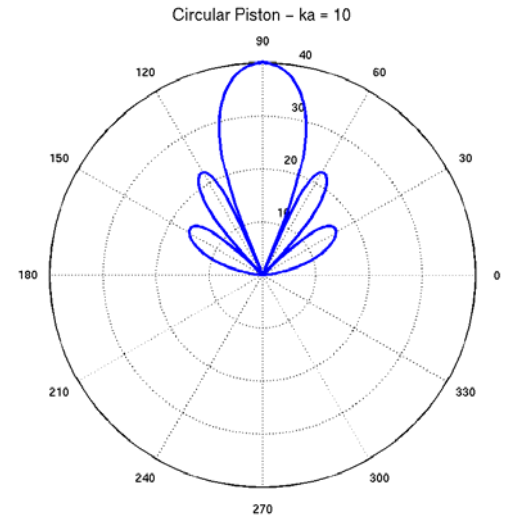
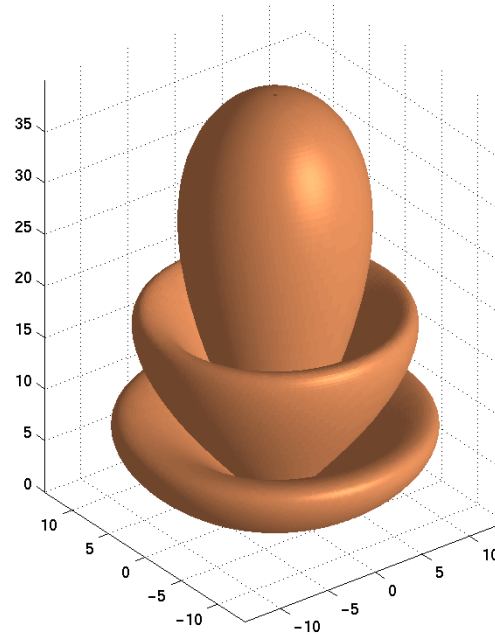
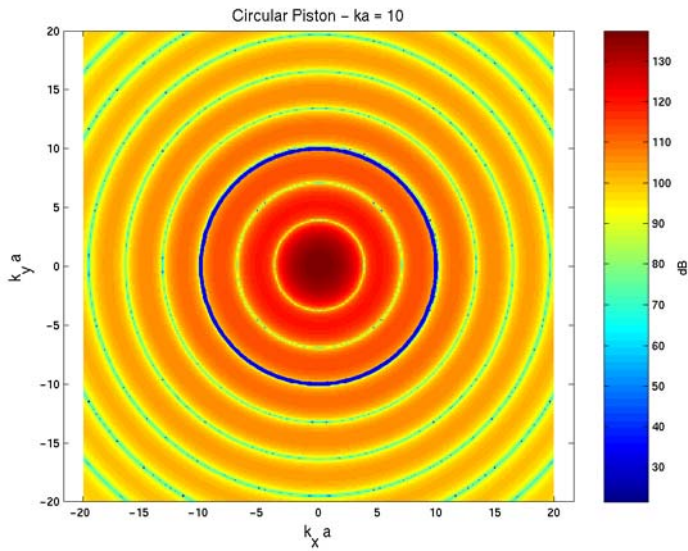
## Directivity Function

$$D(\theta, \phi) = D(\theta) = -i\rho\omega a^2 \frac{J_1(k_r a)}{k_r a}$$



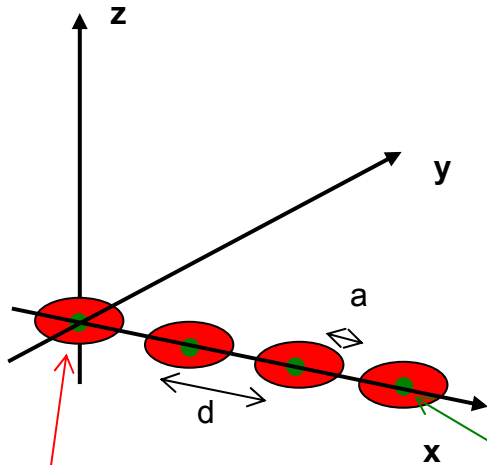
$$f = \omega/2\pi = kc/2\pi$$

Circular Piston - ka = 10





# Array of Baffled Pistons



## Baffled Piston Array

$$\dot{w}_n(x, y, 0) = S_n \dot{w}(x - x_n, y - y_n, 0)$$

## Fourier Transform

$$\dot{w}_n(k_x, k_y, 0) = S_n \dot{w}(k_x, k_y, 0) e^{-ik_x x_n} e^{ik_y y_n}$$

## Directivity Function

$$D(\theta, \phi) = -\frac{i\rho\omega}{2\pi} \dot{w}_n(k_x, k_y, 0)$$

$$= -\frac{i\rho\omega}{2\pi} \dot{w}(k_x, k_y, 0) \sum_{n=1}^N S_n e^{-ik_x x_n} e^{-ik_y y_n}$$

Array of Point Sources

One Baffled Piston

$$= -\frac{i\rho\omega}{2\pi} \dot{w}(k_x, k_y, 0) \sum_{n=1}^N \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} S_n \delta(x - x_n) \delta(y - y_n) e^{-ik_x x} e^{-ik_y y} dx dy$$



## circ\_arr.m

```
%
% MATLAB script for plotting the directivity function for
% an array of circular, baffled pistons

% Parameters:
% k      Wavenumber
% rho    Density
% c      Speed of Sound
% a      Radius of piston of piston
% d      Piston separation
% nd     Number of pistons
% qd     Array of piston strengths

clear
figure(1)
hold off
k=10.0;
rho=1000;
c=1500;
a=1.0;

% Half wavelength spacing, d= pi/k
d=pi/k;
nd=10;
ah=(nd-1)*d/2
xd=[-ah:d:ah]';
kxd_0=k/2;
qd=ones(length(xd),1);
qd=exp(-i*kxd_0*xd);
%qd(2)=-1;
ka=k*a;
figure(1);
kxm=2*ka;
nkx=300;
dkx=2*kxm/(nkx-1);
x=[-kxm:dkx:kxm];
y=x;
o=ones(1,nkx);
kx=x' * o;
ky=(y' * o)';
kr=abs(complex(kx,ky));
kx1=reshape(kx,1,nkx^2);
shd=qd'*exp(-i*xd*kx1);
shd=reshape(shd,nkx,nkx);
ss=rho*k*c*a^2 * besselj(1,kr)./kr;
wavei(dba(ss.*shd)',x,y)
shading('flat')
axis('equal')
b=xlabel('k_x a')
set(b,'FontSize',16);
b=ylabel('k_y a')
set(b,'FontSize',16);

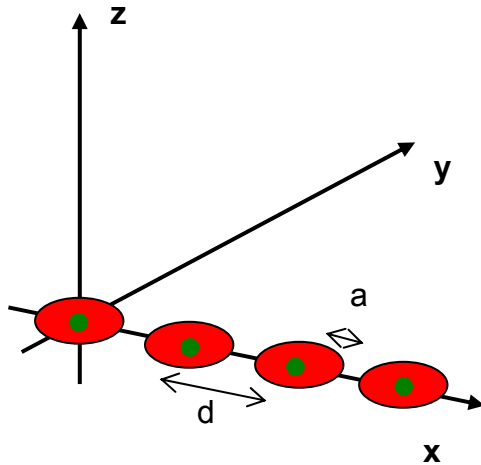
tit=['Circular Piston Array - ka = ' num2str(k*a) ' - d,n = ' num2str(d)
', ' num2str(nd) ]
b=title(tit);
set(b,'FontSize',20);nphi=361;
dphi=2*pi/(nphi-1);
phi=[0:dphi:2*pi];
xx=k*a*cos(phi);
yy=k*a*sin(phi);
hold on
b=plot(xx,yy,'b');
set(b,'LineWidth',3);

figure(2)
nphi=361.
dphi=2*pi/(nphi-1)
nth=181;
dth=0.5*pi/(nth-0.5);

phi=[0:dphi:(nphi-1)*dphi]' * ones(1,nth);
th=( [dth/2:dth:pi/2] '*ones(1,nphi))' ;
kx=ka*sin(th).*cos(phi);
ky=ka*sin(th).*sin(phi);
kr=ka*sin(th);
ss=rho*k*c*a^2*besselj(1,kr)./kr;
kx1=reshape(kx,1,size(kx,1)*size(kx,2));
shd=qd'*exp(-i*xd*kx1);
shd=reshape(shd,size(kx,1),size(kx,2));
ss=dba(ss.*shd);
sm=max(max(ss));
for i=1:size(ss,1)
    for j=1:size(ss,2)
        ss(i,j)=max(ss(i,j),sm-40.0)-(sm-40.0);
    end
end
xx=ss.*sin(th).*cos(phi);
yy=ss.*sin(th).*sin(phi);
zz=ss.*cos(th);
surf1(xx,yy,zz);
colormap('copper');
shading('flat');
axis('equal');
tit=['Circular Piston Array - ka = ' num2str(k*a) ' - d,n = ' num2str(d)
', ' num2str(nd) ]
b=title(tit);
set(b,'FontSize',20);
```



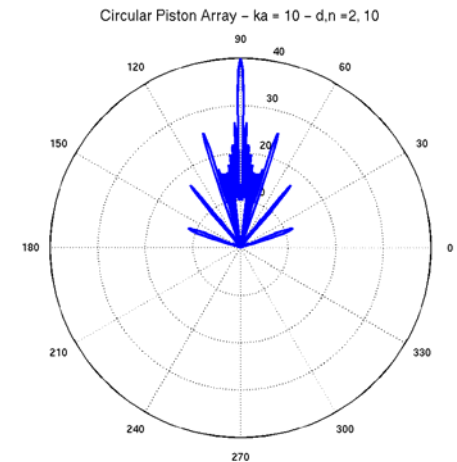
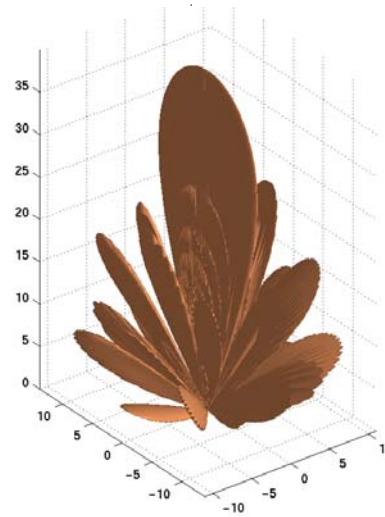
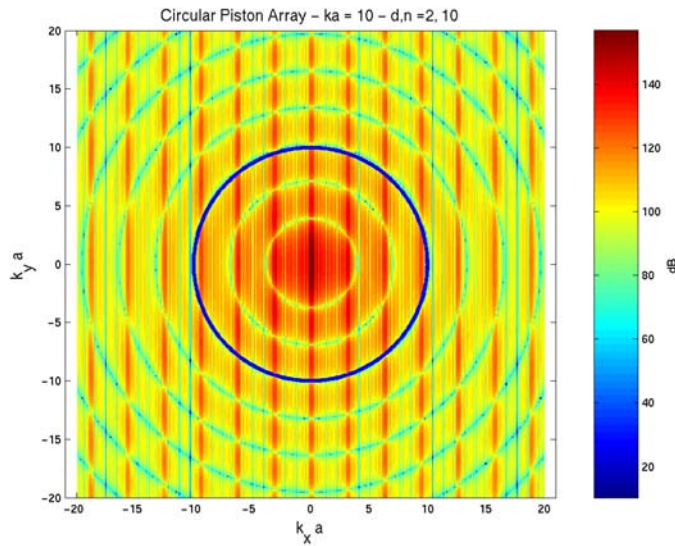
# Array of Circular Pistons



## Directivity Function

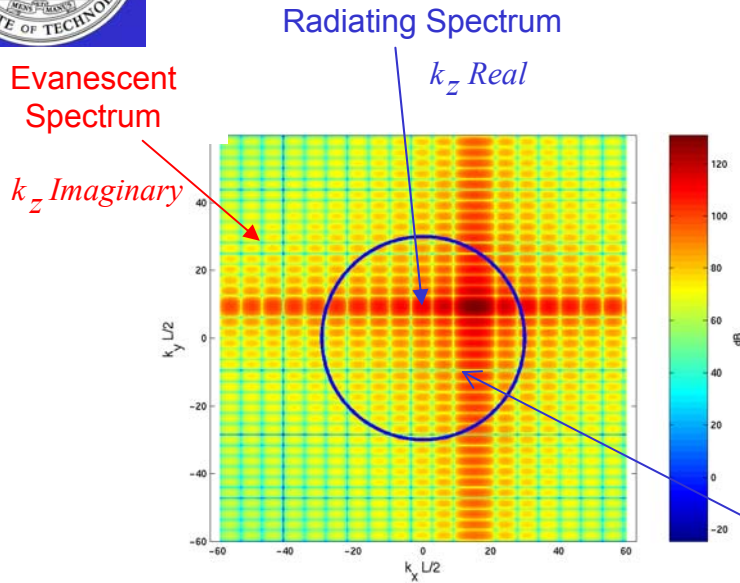
$$\begin{aligned}
 D(\theta, \phi) &= -\frac{i\rho\omega}{2\pi} \sum_{n=1}^N \dot{w}_n(k_x, k_y, 0) \\
 &= -\frac{i\rho\omega}{2\pi} \dot{w}(k_x, k_y, 0) \sum_{n=1}^N S_n e^{-ik_x x_n} e^{-ik_y y_n} \\
 &= -\frac{i\rho\omega}{2\pi} \dot{w}(k_x, k_y, 0) \sum_{n=1}^N \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} S_n \delta(x - x_n) \delta(y - y_n) e^{-ik_x x} e^{-ik_y y} dx dy
 \end{aligned}$$

Circular Piston Array –  $ka = 10$  –  $d, n = 2, 10$





# Radiated Power



$$\Pi(\omega) = \frac{1}{8\pi^2} \text{Re} \left[ \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} p_{\omega}(k_x, k_y; 0) \dot{w}_{\omega}(k_x, k_y; 0) dk_x dk_y \right]$$

$$p_{\omega}(k_x, k_y; 0) = \frac{\rho\omega}{k_z} \dot{w}_{\omega}(k_x, k_y; 0)$$

## Radiated Power

$$\Pi(\omega) = \frac{1}{2} \int \int_S \text{Re}[p_{\omega}(x, y, 0) \dot{w}_{\omega}^*(x, y, 0)] dS$$

## Fourier Transforms

$$p_{\omega}(x, y, 0) = \frac{1}{4\pi^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} p_{\omega}(k_x, k_y; 0) e^{i(k_x x + k_y y)} dk_x dk_y$$

$$\dot{w}_{\omega}^*(x, y, 0) = \frac{1}{4\pi^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \dot{w}_{\omega}(q_x, q_y; 0) e^{-i(q_x x + q_y y)} dq_x dq_y$$

$$\frac{1}{4\pi^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} e^{i(k_x - q_x)x} e^{i(k_y - q_y)y} dx dy = \delta(k_x - q_x) \delta(k_y - q_y)$$

$$\begin{aligned} \Pi(\omega) &= \frac{\rho\omega}{8\pi^2} \text{Re} \left[ \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{|\dot{w}_{\omega}(k_x, k_y; 0)|}{k_z} dk_x dk_y \right] \\ &= \frac{\rho\omega}{8\pi^2} \int_k^k dk_x \int_{-\sqrt{k^2 - k_x^2}}^{\sqrt{k^2 - k_x^2}} \frac{|\dot{w}_{\omega}(k_x, k_y; 0)|}{k_z} dk_y \end{aligned}$$





# Point-Driven Plate Radiation

## Plate Bending Equation

$$D \left( \frac{\partial^4 w}{\partial x^4} + 2 \frac{\partial^4 w}{\partial x^2 \partial y^2} + \frac{\partial^4 w}{\partial y^4} \right) + \rho_s h \frac{\partial^2 w}{\partial t^2} = F(t) \delta(x) \delta(y) - p_a(x, y, t)$$

$$D = \frac{Eh^3}{12(1-\nu^2)}$$

Skudrzyk's number

$$\alpha \equiv \left( \frac{D}{\rho_s h} \right)^{1/4} = \left( \frac{Eh^2}{12\rho_s(1-\nu^2)} \right)^{1/4}$$

## Frequency Domain

$$D \left( \frac{\partial^4 w_\omega}{\partial x^4} + 2 \frac{\partial^4 w_\omega}{\partial x^2 \partial y^2} + \frac{\partial^4 w_\omega}{\partial y^4} \right) + \rho_s h \omega^2 w_\omega = F_\omega \delta(x) \delta(y) - p_a(x, y)$$

## Cylindrical Coordinates

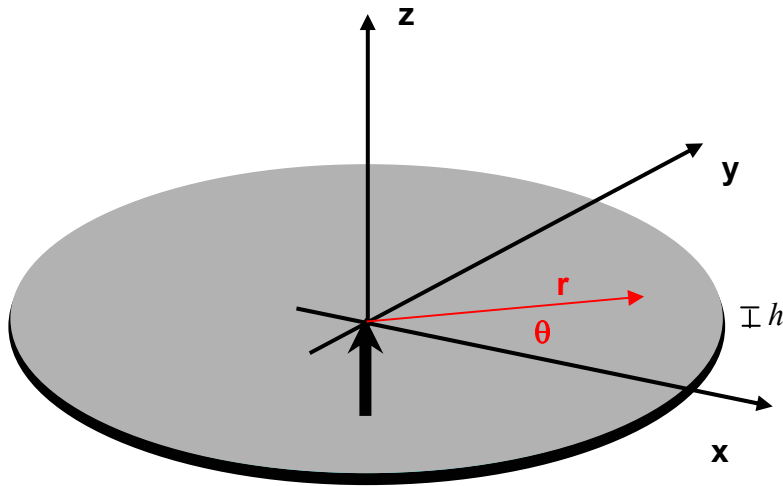
$$x = r \cos \theta$$

$$y = r \sin \theta$$

$$r^2 = x^2 + y^2$$

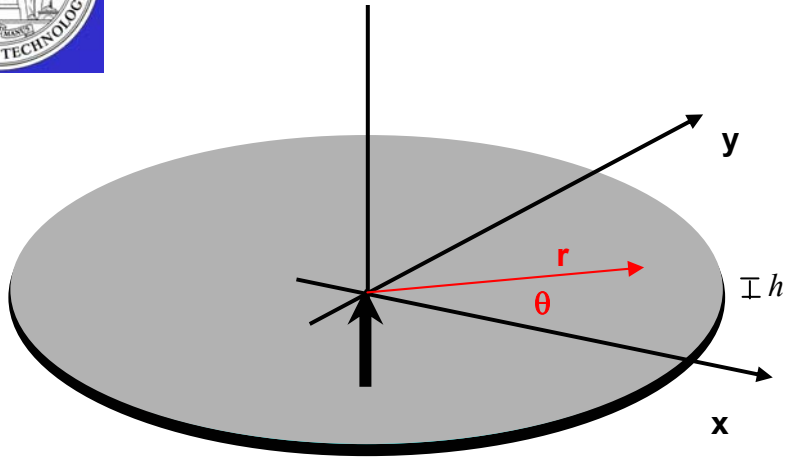
$$D \left( \frac{d^2}{dr^2} + \frac{d}{rdr} \right)^2 w_\omega - \rho_s h \omega^2 w_\omega = F_\omega \frac{\delta(r)}{2\pi r} - p_a(r)$$

$$\left( \frac{d^2}{dr^2} + \frac{d}{rdr} \right)^2 = \left( \frac{d^2}{dr^2} + \frac{d}{rdr} \right) \left( \frac{d^2}{dr^2} + \frac{d}{rdr} \right)$$





# Point-Driven Plate Radiation



## Cylindrical Coordinates

$$D \left( \frac{d^2}{dr^2} + \frac{d}{rdr} \right)^2 w_\omega - \rho_s h \omega^2 w_\omega = F_\omega \frac{\delta(r)}{2\pi r} - p_a \delta(r)$$

$$\left( \frac{d^2}{dr^2} + \frac{d}{rdr} \right)^2 = \left( \frac{d^2}{dr^2} + \frac{d}{rdr} \right) \left( \frac{d^2}{dr^2} + \frac{d}{rdr} \right)$$

## Hankel Transform

$$w(k_r) = \int_0^\infty w(r) J_0(k_r r) r dr$$

$$w(r) = \int_0^\infty w(k_r) J_0(k_r r) k_r dk_r$$

## Hankel Transforms

$$\left( \frac{d^2}{dr^2} + \frac{d}{rdr} \right) J_0(k_r r) = -k_r^2 J_0(k_r r)$$

$$\frac{\delta(r)}{2\pi r} = \int_0^\infty J_0(k_r r) k_r dk_r$$

## Light Fluid Loading

$$D k_r^4 w_\omega(k_r) - \rho_s h \omega^2 w_\omega(k_r) \simeq F_\omega$$

$$w_\omega(k_r) = \frac{F(\omega)}{2\pi D (k_r^4 - k_f^4)}$$

## Flexural Wavenumber

$$k_f = \left( \frac{m_s \omega^2}{D} \right)^{1/4} = \left( \frac{\rho_s h \omega^2}{D} \right)^{1/4}$$

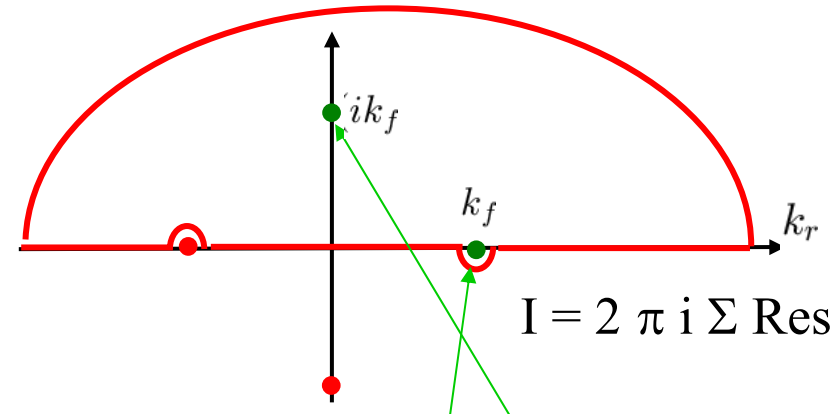
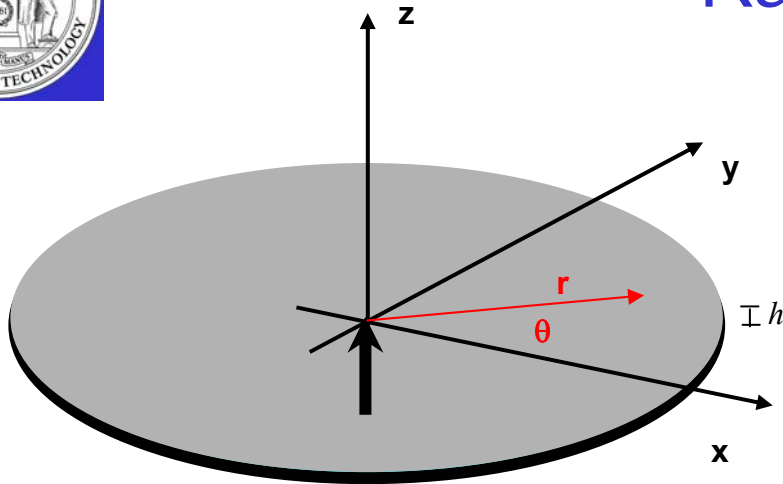
$$k_f = \frac{\omega}{\alpha}$$

## Particle Velocity

$$\dot{w}_\omega(k_r) = \frac{-i\omega F_\omega}{2\pi D (k_r^4 - k_f^4)}$$



# Radiated Field



## Inverse Hankel Transform

$$\begin{aligned}
 w(r) &= \frac{F_\omega}{2\pi D} \int_0^\infty \frac{J_0(k_r r)}{k_r^4 - k_f^4} k_r dk_r \\
 &= \frac{F_\omega}{2\pi D} \int_{-\infty}^\infty \frac{H_0^{(1)}(k_r r)}{k_r^4 - k_f^4} k_r dk_r
 \end{aligned}$$

$$\begin{aligned}
 J_0(x) &= \frac{1}{2} \left( H_0^{(1)}(x) + H_0^{(2)}(x) \right) \\
 &= \frac{1}{2} \left( H_0^{(1)}(x) - H_0^{(1)}(-x) \right)
 \end{aligned}$$

## Complex Contour Integration

$$\begin{aligned}
 \dot{w}_\omega(r) &= \frac{F_\omega}{8\alpha^2 m_s} \left[ H_0^{(1)}(k_f r) - H_0^{(1)}(ik_f r) \right] \\
 &= \frac{F_\omega}{8\alpha^2 m_s} \left[ H_0^{(1)}(k_f r) - \frac{2i}{\pi} K_0(k_f r) \right]
 \end{aligned}$$

$$H_0^{(1)}(k_r r) \rightarrow \sqrt{\frac{2}{\pi k_r r}} e^{i(k_r r - \pi/4)}$$

## Drive-point Impedance

$$Z_p = F_\omega / \dot{w}(0) = 8\alpha^2 m_s$$

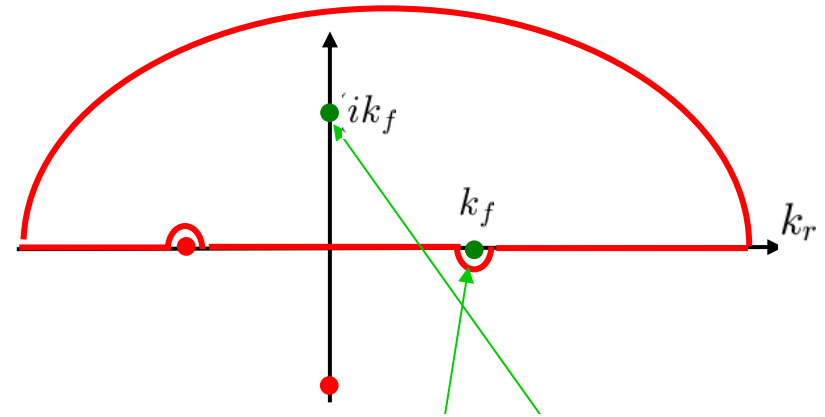
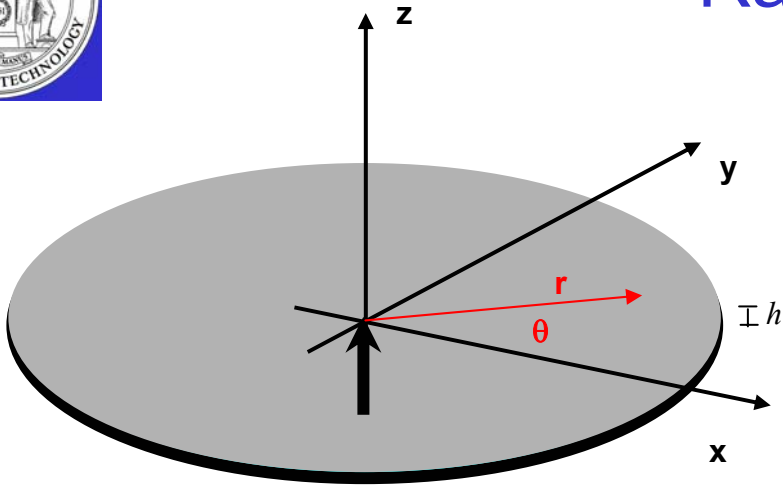
## Flexural Wave Speed

$$k_f = \omega / c_f$$

$$c_f = \omega / k_f = \alpha \sqrt{\omega}$$



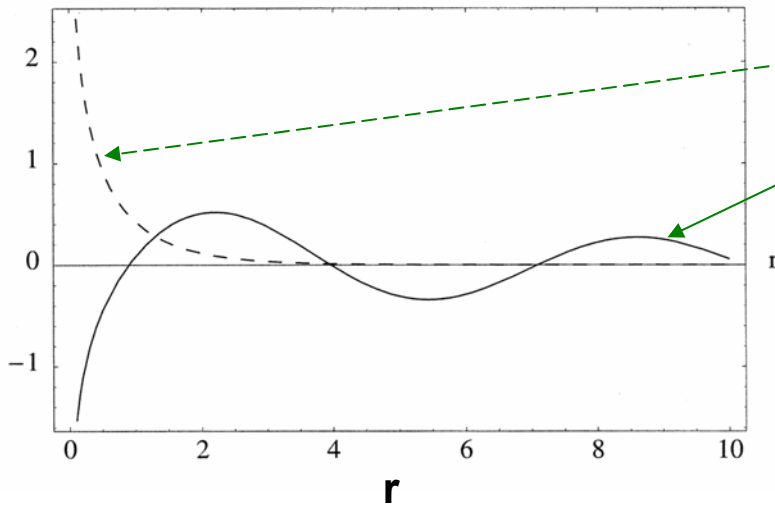
# Radiated Field



## Complex Contour Integration

$$\dot{w}_\omega(r) = \frac{F_\omega}{8\alpha^2 m_s} \left[ H_0^{(1)}(k_f r) - H_0^{(1)}(ik_f r) \right]$$

$$= \frac{F_\omega}{8\alpha^2 m_s} \left[ H_0^{(1)}(k_f r) - \frac{2i}{\pi} K_0(k_f r) \right]$$



$$H_0^{(1)}(k_r r) \rightarrow \sqrt{\frac{2}{\pi k_r r}} e^{i(k_r r - \pi/4)}$$

## Drive-point Impedance

$$Z_p = F_\omega / \dot{w}(0) = 8\alpha^2 m_s$$

## Flexural Wave Speed

$$k_f = \omega / c_f$$

$$c_f = \omega / k_f = \alpha \sqrt{\omega}$$



# Far Field Radiation

$$p(R, \theta, \phi) = -\frac{i\rho\omega}{2\pi} \frac{e^{ikR}}{R} \dot{w}_\omega(k_r) = -\frac{i\rho\omega}{2\pi} \frac{e^{ikR}}{R} \dot{w}_\omega(k \sin\theta)$$

$$\sin \theta_0 = k_f / k$$

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See Figure 2.23 in Williams, E. G. *Fourier Acoustics*.  
London: Academic Press, 1999

$$k < k_f$$

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See Figure 2.24 in [Williams].

