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2.004 Dynamics and Control II
Spring 2008

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Lecture 18¹

Reading:

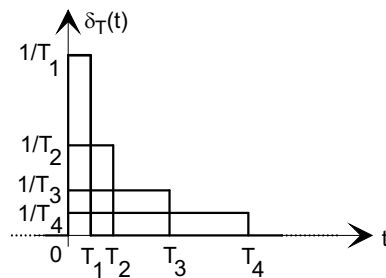
- Nise: Sec. 1.5

1 Common Inputs Used in Control System Design and Analysis

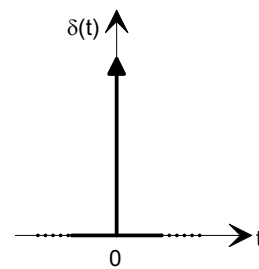
Two classes of inputs commonly used to characterize the performance of feedback control systems are:

(a) **The “Singularity” Functions:** These functions have a discontinuity at time $t = 0$:

- (i) **The Dirac Delta (Impulse) Function:** The delta function is used to characterize the response of a system to brief, intense inputs. In the figure below, (a) shows some unit pulses (pulses with unit area so that if the duration of the pulse is T , its amplitude is $1/T$). The Dirac delta function $\delta(t)$ is the limiting case of such pulses as $T \rightarrow 0$. Notice that this implies that the amplitude $1/T \rightarrow \infty$.



a) Unit pulses of different extents



b) The impulse function

The strict definition of $\delta(t)$ is

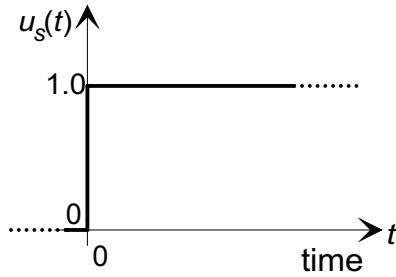
$$\delta(t) = 0, \quad \text{for } t \neq 0$$

$$\delta(t) \text{ is undefined at } t = 0 \quad \left(\lim_{t \rightarrow 0} \delta(t) = \infty \right)$$

$$\int_{0^-}^{0^+} \delta(t) dt = 1$$

- (ii) **The Unit-Step Function $u_s(t)$:** The unit-step (or Heaviside) function is used to characterize a system’s transient response to a sudden change.

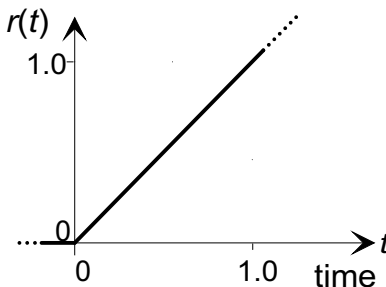
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The definition is

$$\begin{aligned}
 u_s(t) &= 0 \quad \text{for } t < 0 \\
 &= 1 \quad \text{for } t > 0
 \end{aligned}$$

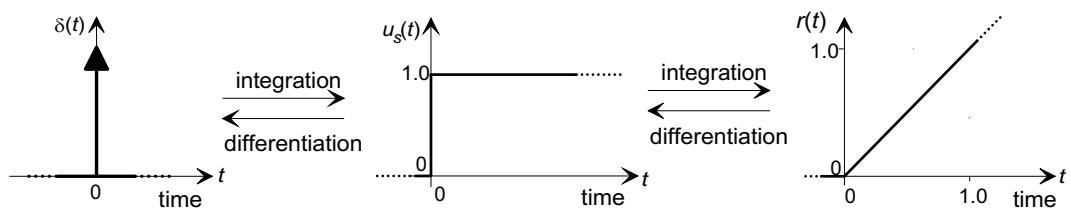
(iii) **The Unit-Ramp Function $r(t)$:** The unit-ramp function is used to characterize a system's ability to follow a time-varying input, and the transient behavior around a discontinuity in the slope of an input function.



The definition is

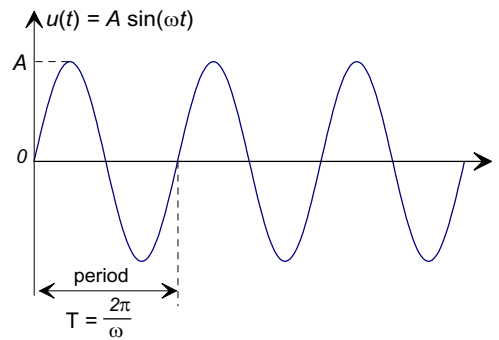
$$\begin{aligned}
 r(t) &= 0 \quad \text{for } t < 0 \\
 &= t \quad \text{for } t > 0
 \end{aligned}$$

The singularity functions are related to each other by differentiation and integration, as shown below:



(b) **Sinusoidal Inputs:** The response of linear systems to sinusoidal inputs of the form

$$u(t) = A \sin(\omega t + \theta)$$

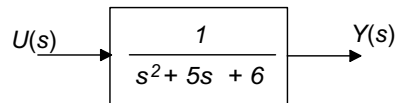


is of fundamental importance to control engineering and system dynamics and will be studied extensively throughout the course.

■ Example 1

In practice a machine, described a second-order transfer function $G(s)$, will be subjected to inputs that change suddenly. Use the unit-step response to determine how long it will take the machine's response to settle to a new steady-state value after a change.

The system's block diagram is



and the governing differential equation is

$$\frac{d^2y}{dt^2} + 5\frac{dy}{dt} + 6y = u(t).$$

The step response assumes that the system is “at rest” at time $t = 0$, that is $y(0) = 0$ and $\dot{y}(0) = 0$, and that the input $u(t) = u_s(t)$.

The solution is

$$y(t) = y_h(t) + y_p(t)$$

where $y_h(t)$ is the *homogeneous solution*, and $y_p(t)$ is the *particular integral*. The characteristic equation is

$$\lambda^2 + 5\lambda + 6 = (\lambda + 3)(\lambda + 2) = 0$$

and

$$y_h(t) = C_1e^{-3t} + C_2e^{-2t}.$$

Assume $y_p(t) = K$ and substitute into the differential equation

$$0 + 0 + 6K = 1$$

or $y_p(t) = 1/6$. The complete solution is

$$y(t) = C_1 e^{-3t} + C_2 e^{-2t} + 1/6.$$

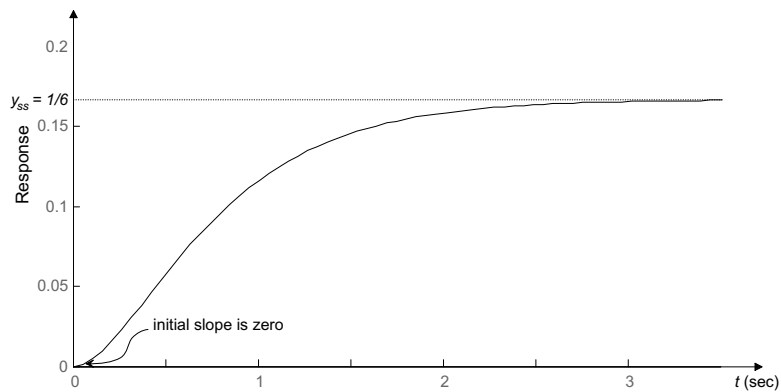
At time $t = 0$

$$\begin{aligned} y(0) &= C_1 + C_2 + 1/6 = 0 \\ \dot{y}(0) &= -3C_1 - 2C_2 + 0 = 0 \end{aligned}$$

giving $C_1 = 1/3$ and $C_2 = -1/2$, so that the system's response to a unit-step input is

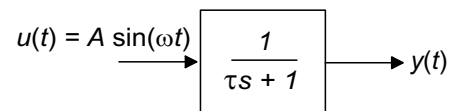
$$y_{step}(t) = \frac{1}{3}e^{-3t} - \frac{1}{2}e^{-2t} + 1/6.$$

The response is shown below, and indicates that it takes this system 2.5–3 seconds to respond to the step.



■ Example 2

Find the steady-state response of a first-order system to a sinusoidal input $u(t) = A \sin(\omega t)$.



The differential equation is

$$\tau \frac{dy}{dt} + y = u(t)$$

and assume the complete solution is $y(t) = y_h(t) + y_p(t)$ as in the previous example. The characteristic equation is

$$\tau \lambda + 1 = 0$$

from which

$$y_h(t) = Ce^{-t/\tau}$$

and assume

$$y_p(t) = K_1 \cos(\omega t) + K_2 \sin(\omega t)$$

In steady-state we assume that $y_h(t) = Ce^{-t/\tau}$ has decayed to zero, and

$$y_{ss}(t) = y_p(t) = K_1 \cos(\omega t) + K_2 \sin(\omega t)$$

Substitution of $y_p(t)$ into the differential equation gives

$$\tau\omega(-K_1 \sin(\omega t) + K_2 \cos(\omega t)) + (K_1 \cos(\omega t) + K_2 \sin(\omega t)) = A \sin(\omega t)$$

or

$$(\omega\tau K_2 + K_1) \cos(\omega t) + (-\omega\tau K_1 + K_2) \sin(\omega t)$$

and comparing coefficients

$$\begin{aligned}\omega\tau K_2 + K_1 &= 0 \\ -\omega\tau K_1 + K_2 &= A,\end{aligned}$$

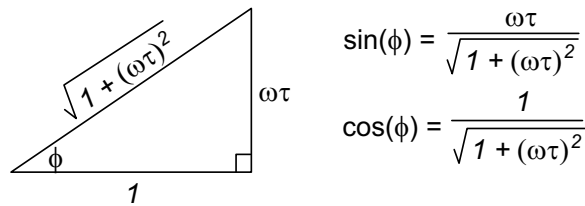
or

$$K_1 = \frac{\omega\tau A}{1 + (\omega\tau)^2}, \quad K_2 = \frac{A}{1 + (\omega\tau)^2}$$

so that

$$\begin{aligned}y_{ss}(t) &= y_p(t) = \frac{A}{1 + (\omega\tau)^2} (\sin(\omega t) - \omega\tau \cos(\omega t)) \\ &= \frac{A}{\sqrt{1 + (\omega\tau)^2}} \left(\frac{1}{\sqrt{1 + (\omega\tau)^2}} \sin(\omega t) - \frac{\omega\tau}{\sqrt{1 + (\omega\tau)^2}} \cos(\omega t) \right) \\ &= \frac{A}{\sqrt{1 + (\omega\tau)^2}} (\cos(\phi) \sin(\omega t) - \sin(\phi) \cos(\omega t)).\end{aligned}$$

using the following triangle



Then the system sinusoidal response is

$$y_{ss}(t) = \frac{A}{\sqrt{1 + (\omega\tau)^2}} \sin(\omega t - \phi)$$

where $\phi = \tan^{-1}(\omega\tau)$. We note the following

- (a) The steady-state sinusoidal response is a sinusoid of the same frequency as the input.
- (b) There is a phase shift (lag) between the input and output $\phi = \tan^{-1}(\omega\tau)$.
- (c) The amplitude of the output is a function of the input frequency ω .
- (d)
- At low frequencies ($\omega \rightarrow 0$), the response is $y_{ss}(t) \approx A \sin(\omega t)$ and the amplitude approaches that of the input.
 - At very high frequencies ($\omega \rightarrow \infty$), the response is $y_{ss}(t) \approx (A/\omega\tau) \sin(\omega t - \pi/2)$ and the response amplitude becomes very small.
 - When $\omega = 1/\tau$, $y_{ss}(t) = (A/\sqrt{2}) \sin(\omega t - \pi/4)$, that is the amplitude is reduced by a factor of 0.707, and the phase shift is 45° .
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