

STRUCTURE- PROPERTY RELATIONSHIP IN TITANIUM FOAMS

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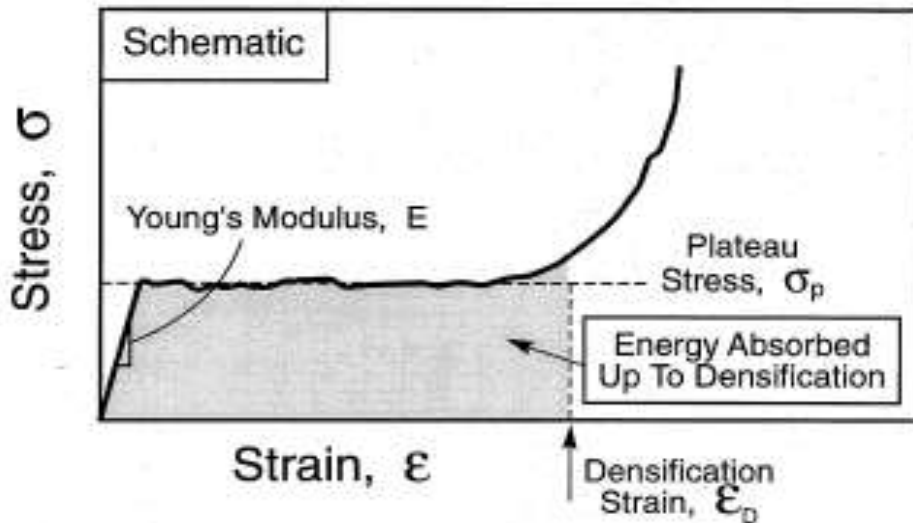
WHY CELLULAR MATERIALS?

“When modern man builds large load-bearing structures, he uses dense solids: steel, concrete, glass.

When Nature does the same, she generally uses cellular materials: wood, bone, coral.

There must be good reasons for it.”

M. F. Ashby, University of Cambridge

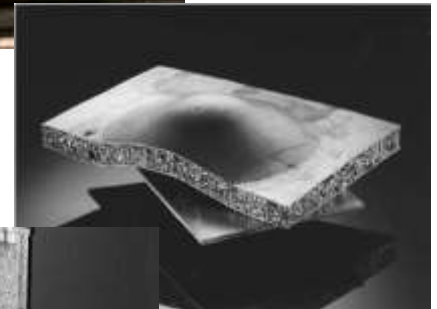


A.G. Evans, J.W. Hutchinson, M.F. Ashby, *Multifunctionality of cellular metal systems*, *Progress in Materials Science*, 43, 1999, 171-221.

Source: Evans, A. G., J. W. Hutchinson, et al. *Progress in Materials Science* 43 (1999): 171-221.

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<http://www.sciencedirect.com/science/article/pii/S0079642598000048>



Source (middle figure): Banhart, J. "Manufacture, Characterisation and Application of Cellular Metals and Metal Foams." *Progress in Materials Science* 46 (2001): 559-632. Courtesy of Elsevier. Used with permission.

WHY TITANIUM?

- ✓ Low density (4.54 g/cm³)
- ✓ High specific strength
- ✓ Excellent corrosion resistance
- ✓ High fatigue resistance
- ✓ High service temperature
- ✓ Biocompatibility

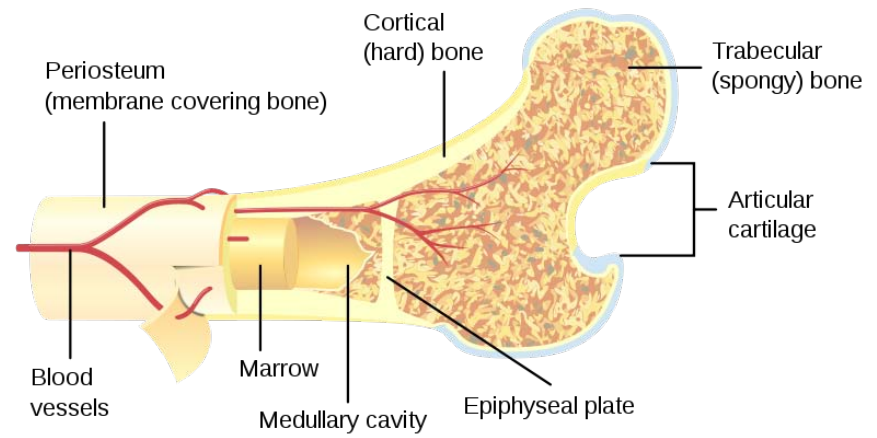


Diagram courtesy of [Pbroks13](#) on Wikimedia Commons. License: CC-BY.

WHY POROUS TITANIUM?

Bone-like stiffness to avoid stress shielding

Higher surface area, roughness and interconnected pores enhance osteointegration and promote a fast healing.

High service temperature + high energy absorption capacity for space applications.

DESIRED IMPLANT PROPERTIES

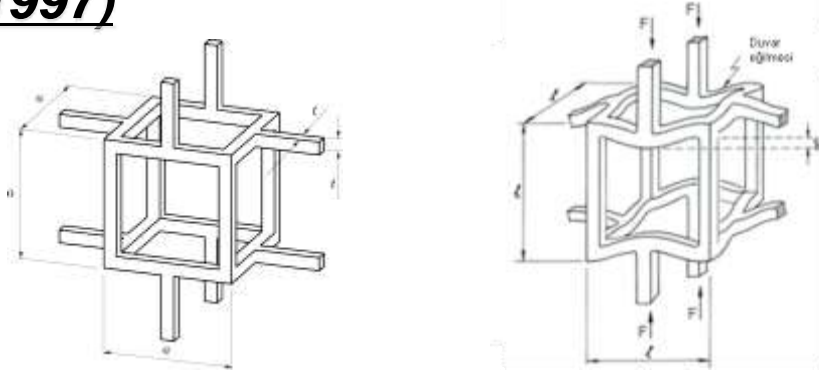
- ✓ Biocompatibility
- ✓ High surface area for cell adhesion
- ✓ Pore interconnectivity for vascularisation
- ✓ Adequate mechanical property to avoid stress shielding
- ✓ High corrosion, fatigue and wear resistance
- ✓ Surface roughness
- ✓ Pores greater than 100-150 μm

The desired structural and mechanical properties of the implant strongly depend on **substituted bone**, the **age** and **daily activity** of the patient.

Property	Age (years)						
	10 - 20	20 - 30	30 - 40	40 - 50	50 - 60	60 - 70	70 - 80
Ultimate strength (MPa)							
Tension	114	123	120	112	93	86	86
Compression	-	167	167	161	155	145	-
Bending	151	173	173	162	154	139	139
Torsion	-	57	57	52	52	49	49
Ultimate strain (%)							
Tension	1.5	1.4	1.4	1.3	1.3	1.3	1.3
Compression	-	1.9	1.8	1.8	1.8	1.8	-
Torsion	-	2.8	2.8	2.5	2.5	2.7	2.7

MECHANICAL PROPERTY PREDICTION

- ✓ Dimensional arguments based on a single unit cell – ***Gibson & Ashby (1997)***



$$\frac{\sigma^*}{\sigma_s} = C_1 \left(\frac{\rho^*}{\rho_s} \right)^{\frac{3}{2}} \quad \frac{E^*}{E_s} = C_2 \left(\frac{\rho^*}{\rho_s} \right)^2$$

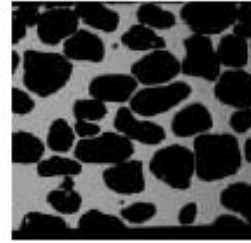
Gibson, L. J., and M. F. Ashby. *Cellular Solids: Structure and Properties*. 2nd ed. Cambridge University Press. © 1997. Figures courtesy of Lorna Gibson and Cambridge University Press.

- ✓ Models on periodic cellular geometries- ***Christensen (1986), Grenestedt (1998), Zhu (1997)***
- ✓ Spatially periodic arrangement of random Voronoi cells using FEM – ***Kraynik (1988), Roberts, Garboczi (2001)***

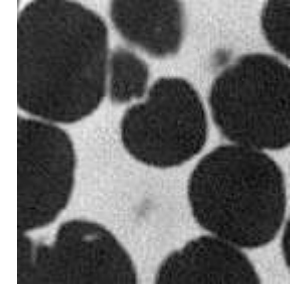
Well defined structures → Expensive

RANDOM FOAMS : IMPERFECTIONS DUE TO PROCESSING

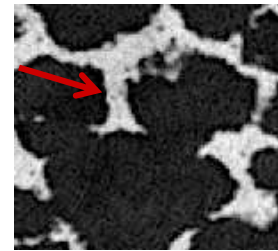
Random cell geometry



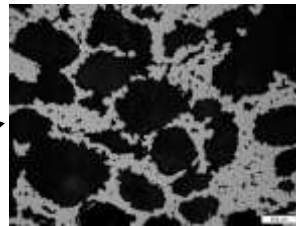
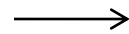
Non-uniform cell wall thickness



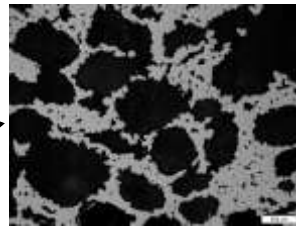
Non load bearing struts



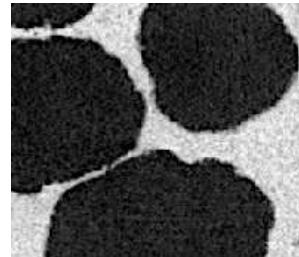
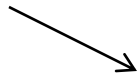
Porous cell walls



Cell wall corrugation



Cell wall curvature



Source: Tuncer, Nihan. "Structure-property Relationship in Titanium Foams", PhD dissertation, Anadolu University, Turkey, 2011.

APPROACH

Statistical approach (based on experiment)

Define the effective structural parameters



Produce tailored architected foams



Measure structural and mechanical props



Relate them to determine the dominant structural features

Structural / Architectural properties

- ✓ Pore size
- ✓ Pore wall thickness
- ✓ Pore wall density
- ✓ Pore sphericity
- ✓ Pore aspect ratio
- ✓ Closed pore fraction
- ✓ Interconnect size
- ✓ Specific surface area

PRODUCTION: POWDER METALLURGY WITH SPACE HOLDERS

- Space holder powders
- Titanium powders ($d_{50}=22\ \mu\text{m}$)

Spacer types

AHC

**Carbamide
(urea)**

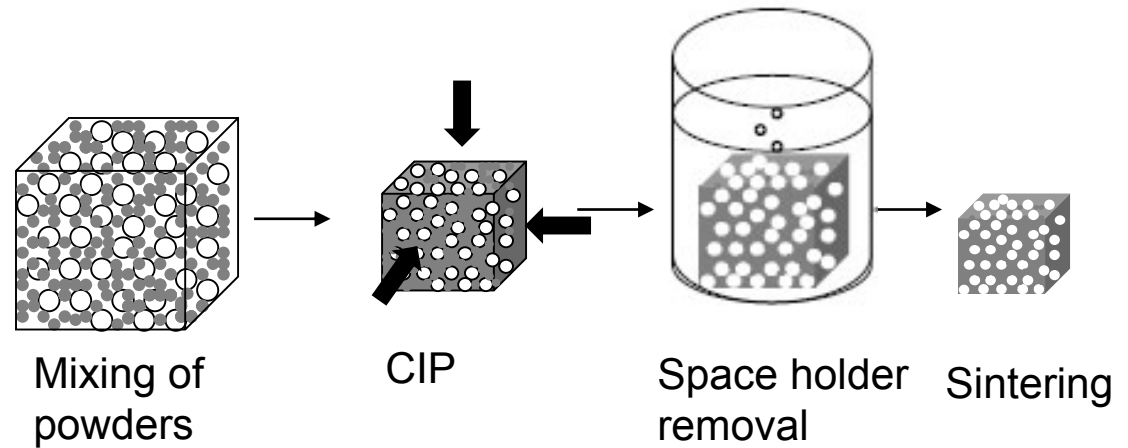
NaCl

KCl

KNO_3

NaNO_3

Mg



Images removed due to copyright restrictions. See Figures 3a and 3: Tuncer, N., and G. Arslan.
[Designing Compressive Properties of Titanium Foams](#). *Journal of Materials Science* 44 (2009): 1477–84.

STRUCTURE-PROPERTY RELATIONSHIP

Powder & process variables



Foam architecture



Mechanical properties

Process

Temperature

Atmosphere

Effect on sintering

- Wall densification
- O₂ diffusion through titanium
- Cell shrinkage

Effect on foam architecture

- Cell wall porosity
- Cell size
- Cell wall thickness

Titanium

Size distribution

- Compaction efficiency
- Wall densification
- Cell and wall size distribution

- Cell wall porosity
- Liquid and gas permeability

Spacer

Amount

Size

Shape

- Compaction efficiency
- Sintering shrinkage
- Cell wall densification

- Relative density (%)
- Cell size
- Cell shape
- Specific surface area
- Connectivity
- Cell wall porosity

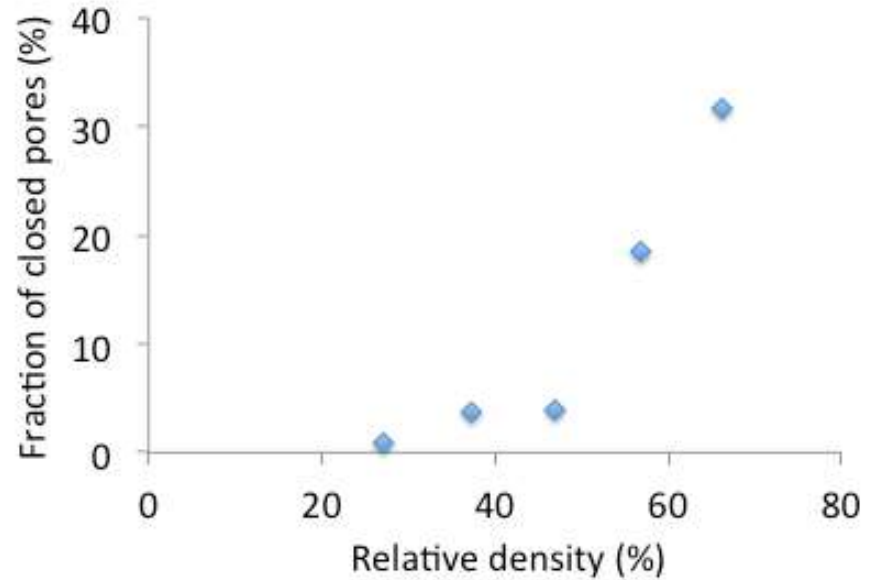
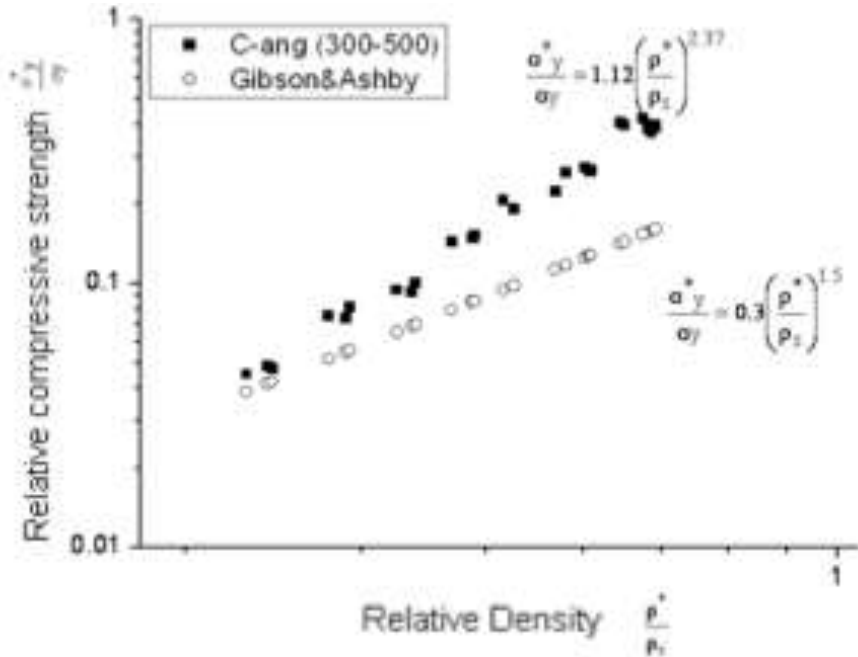
POROSITY IS THE MOST EFFECTIVE PROPERTY

Porosity : 29 – 80 %
Compressive Strength : 25 - 270 MPa
Elastic Modulus : 2.5 – 15 GPa
Pore size : 100 – 1750 μm

Images removed due to copyright restrictions. See Figure 5: N. Tuncer, G. Arslan. [Designing Compressive Properties of Titanium Foams](#). *Journals of Materials Science* 44 (2009), pp. 1477–84.

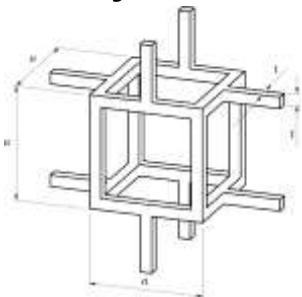
	σ_y (MPa)	E (GPa)
Cortical bone	80-120	3-30
Trabecular bone	2-12	0.05-0.5

POROSITY = MECHANICAL PROPERTY



Source: Tuncer, Nihan. "Structure-property Relationship in Titanium Foams", PhD dissertation, Anadolu University, Turkey, 2011.

Higher dependency on relative density



$$\Rightarrow \frac{\rho}{\rho_s} \approx \left(\frac{t}{a}\right)^2$$

Fraction of closed pores increase with relative density

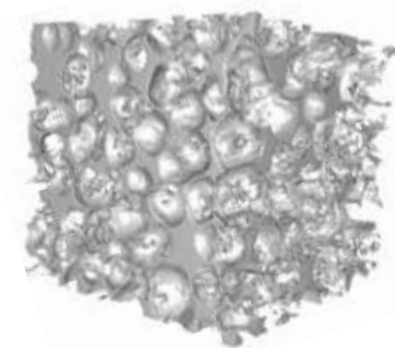
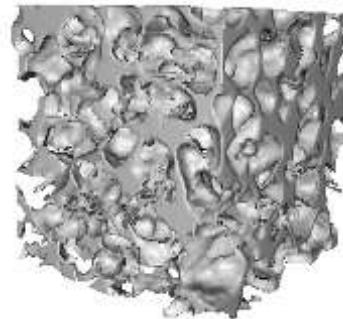
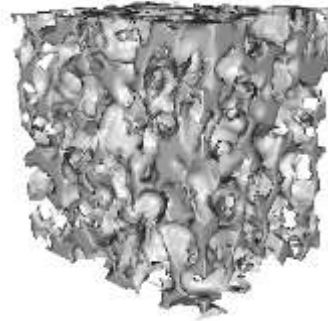
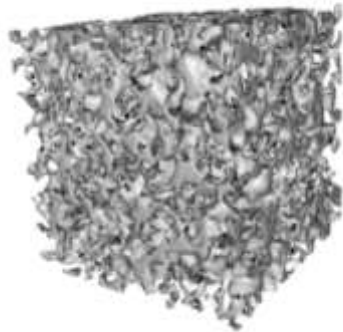
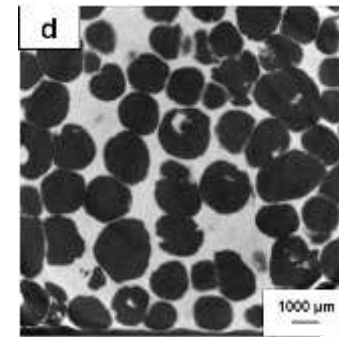
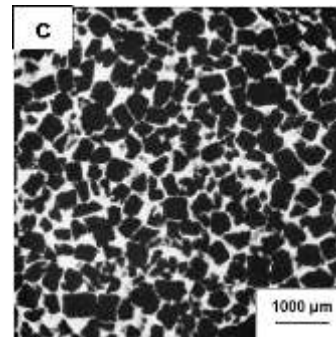
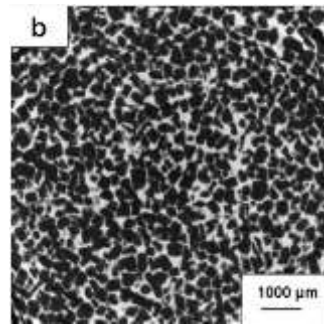
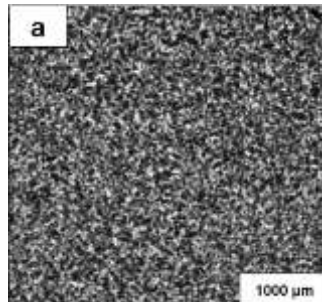
Transition from open cell to partially closed cell with increasing density.

PORE SIZE

ON

**ARCHITECTURAL & MECHANICAL
PROPERTIES**

SPACER SIZE ↔ PORE SIZE



140 μm

375 μm

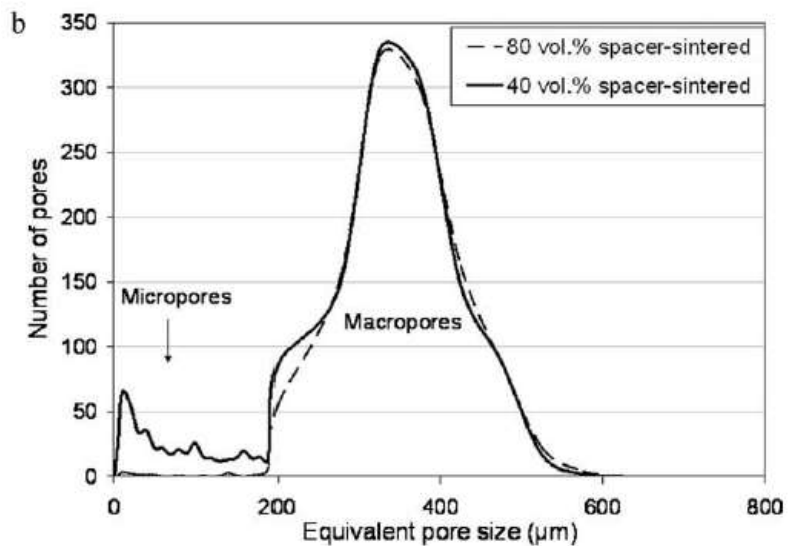
575 μm

1750 μm

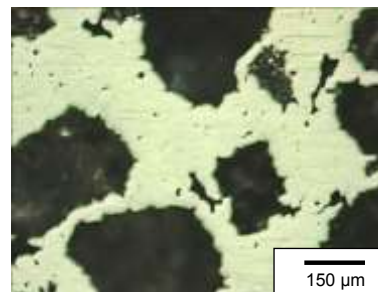
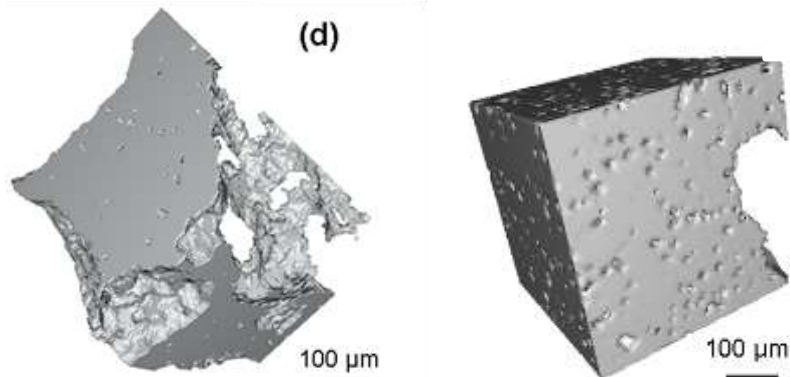
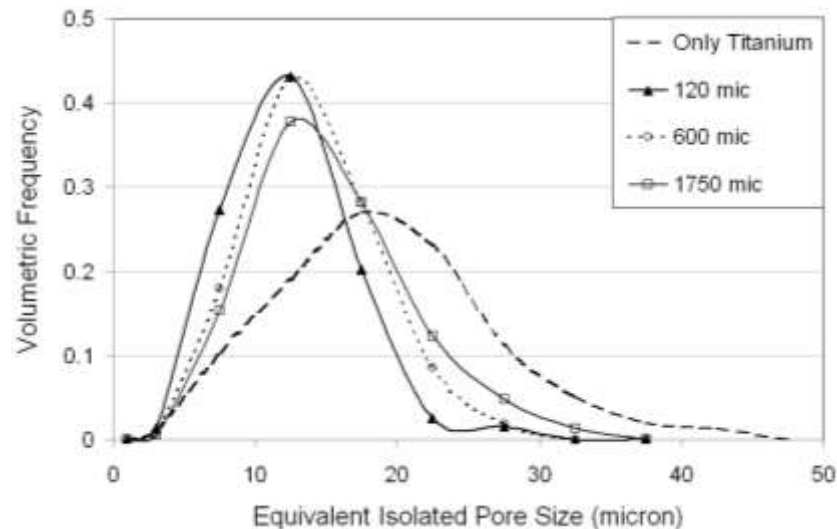
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SPACER SIZE ↔ PORE SIZE

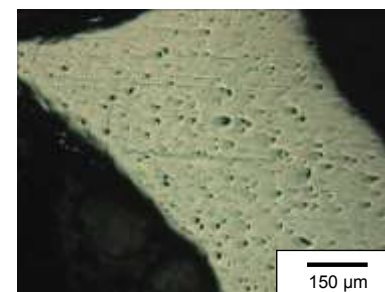
Spacer amount



Spacer size



375 μm



1750 μm

3D rendering of the pore wall parts of the foams produced with **80 vol. %** spacer.

3D rendering of the pore wall parts of the foams produced with **40 vol. %** spacer.

Use of coarser spacers results in less dense cell walls.

Figures courtesy of Elsevier. Used with permission. Source: Tuncer, N., G. Arslan, et al. "Investigation of Spacer Size Effect on Architecture and Mechanical Properties of Porous Titanium". *Materials Science and Engineering A* 530 (2011): 633–42.

PORE SIZE - MECHANICAL PROPERTIES

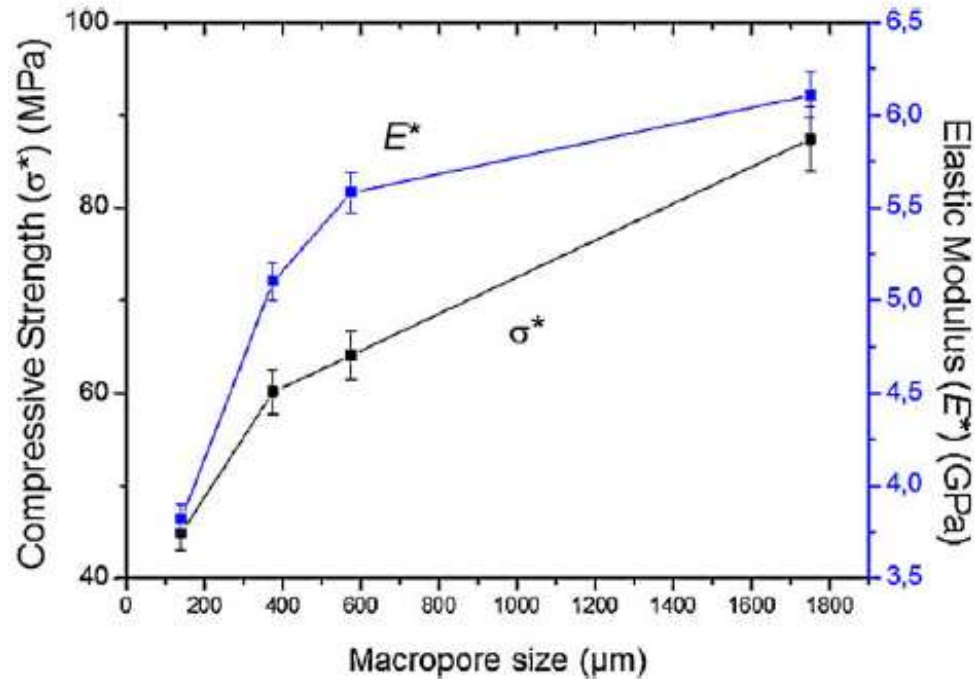
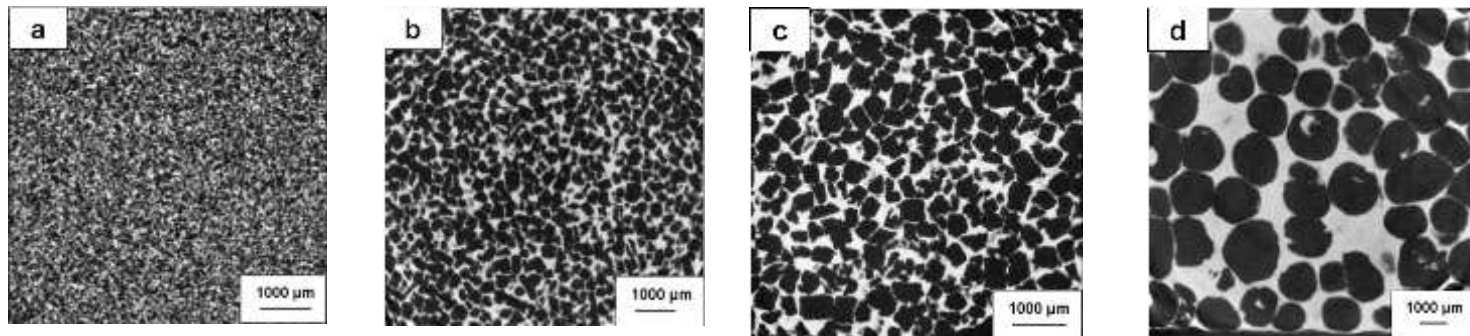


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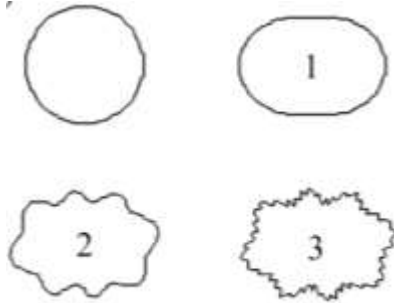
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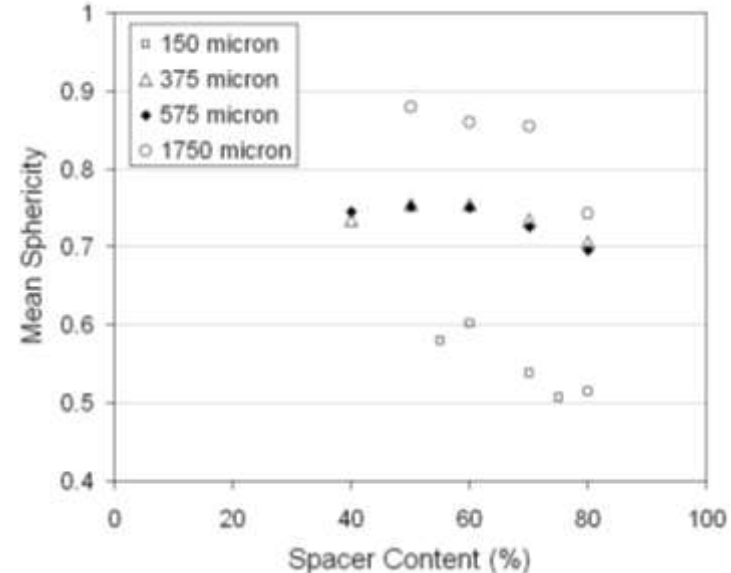
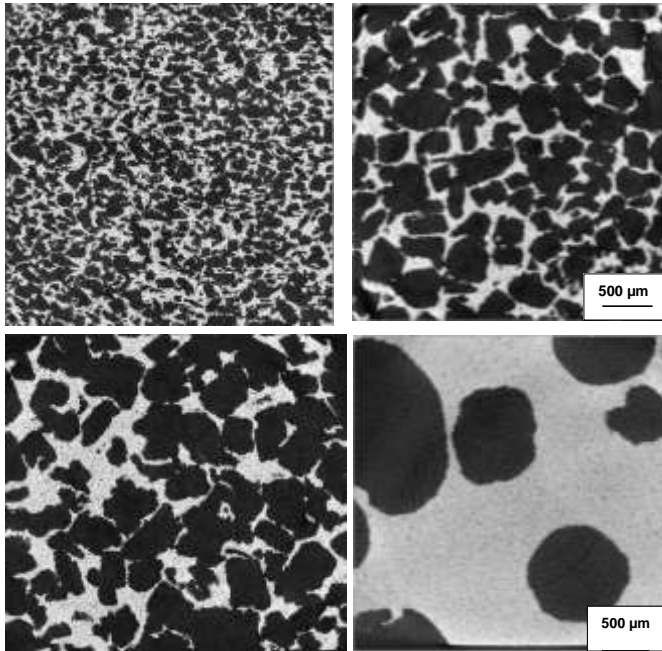
PORE SIZE - MECHANICAL PROPERTIES

Pore sphericity / pore face roughness



$$S = 6V \sqrt{\frac{\pi}{A^3}}$$

$$S_0 > S_1 > S_2 > S_3$$



When the spacers used in this study considered, sphericity, consequently cell face roughness decreases with decreasing spacer size.

$$\sigma (140 \mu\text{m}) < \sigma (375 \mu\text{m}) < \sigma (575 \mu\text{m}) < \sigma (1750 \mu\text{m})$$

PORE SIZE - MECHANICAL PROPERTIES

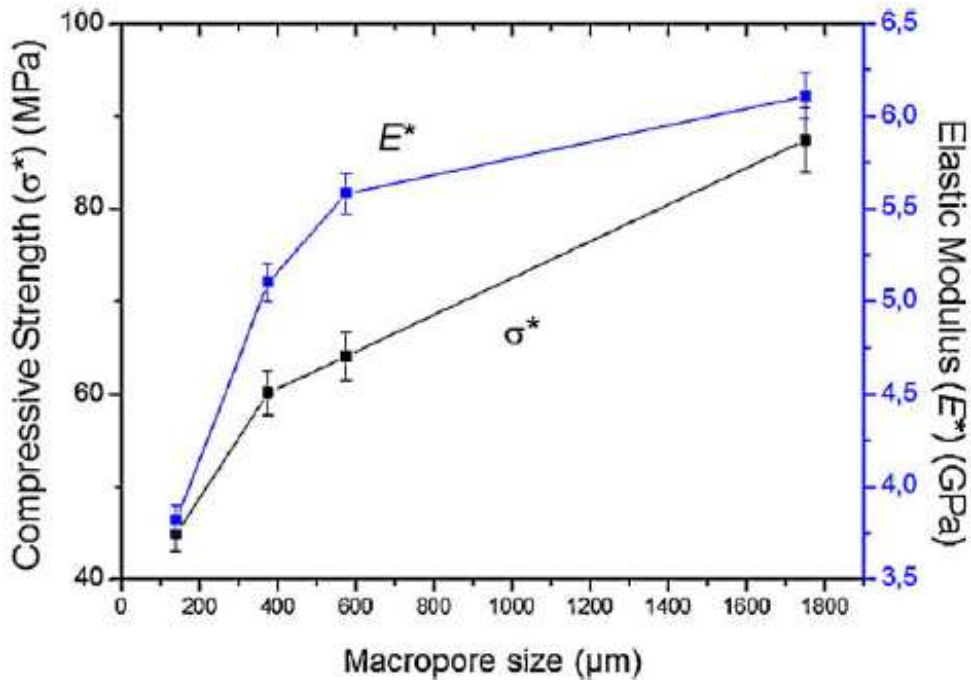
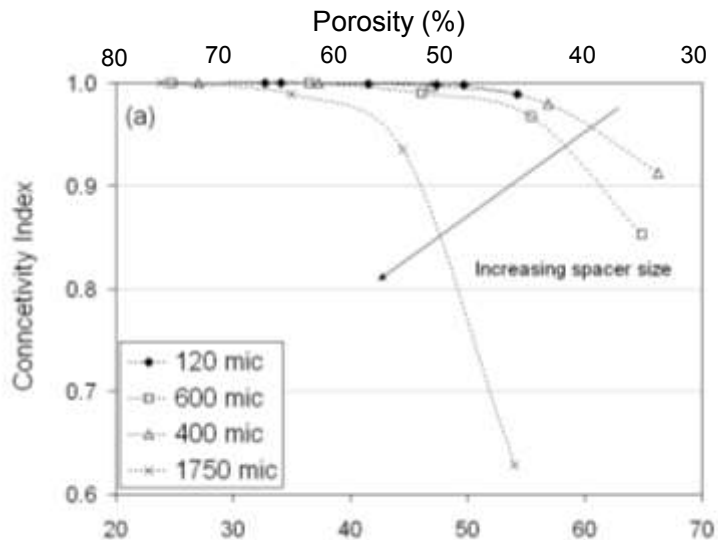


Figure courtesy of Elsevier. Used with permission. Source: Tuncer, N., G. Arslan, et al. "Investigation of Spacer Size Effect on Architecture and Mechanical Properties of Porous Titanium". *Materials Science and Engineering A* 530 (2011): 633–42.

$$\frac{\sigma^*}{\sigma_s} = 0.99 \left(\frac{\rho^*}{\rho_s} \right)^{1.5} + 0.1D - 0.159 \quad R^2 = 0.949$$

ARCHITECTURAL PROPERTIES

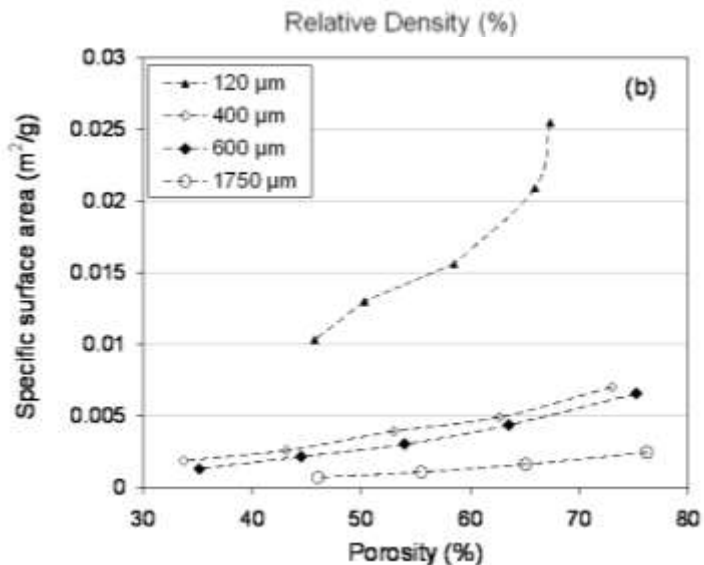
Important properties in terms of permeability and vascularization.



Pore connectivity drops along with porosity

Drop rate is faster in large-pored foams

Foams having average pore sizes below 400 μm are 90 % interconnected down to 30 % porosity.



Specific surface area increases with porosity – decreases with increasing pore size

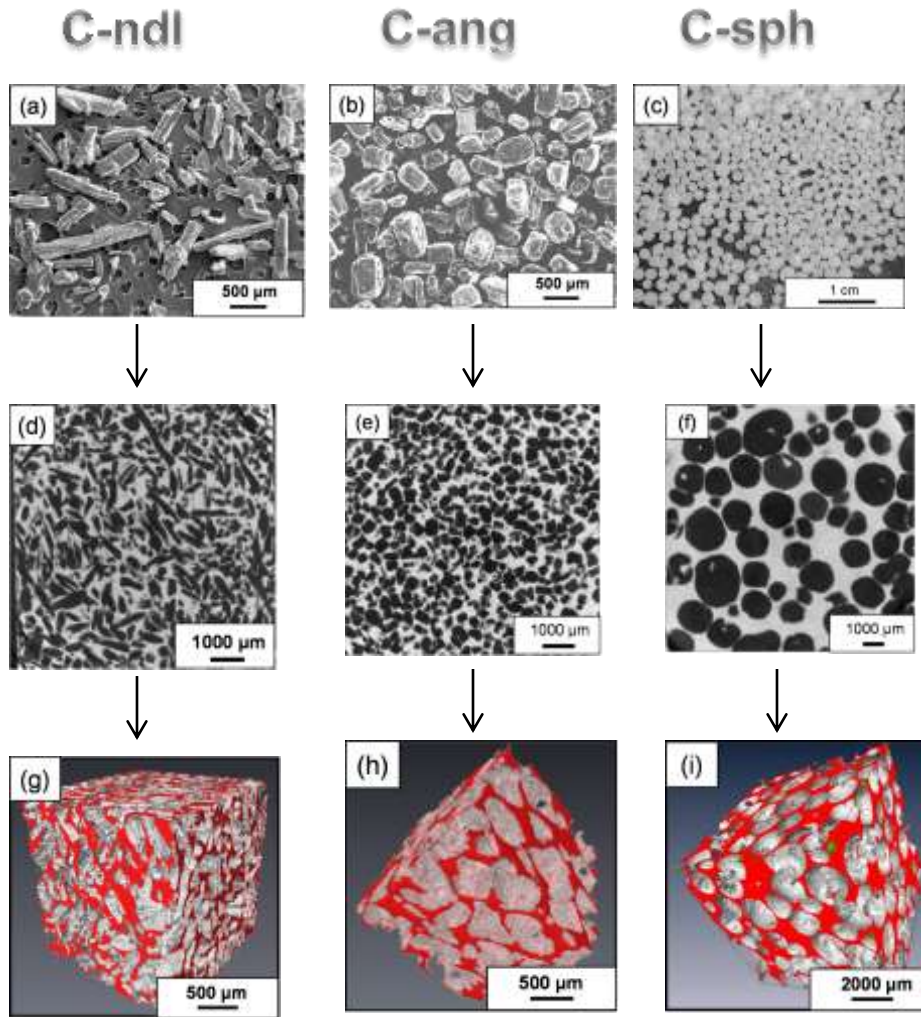
Increase rate is faster in small-pored foams

PORE MORPHOLOGY

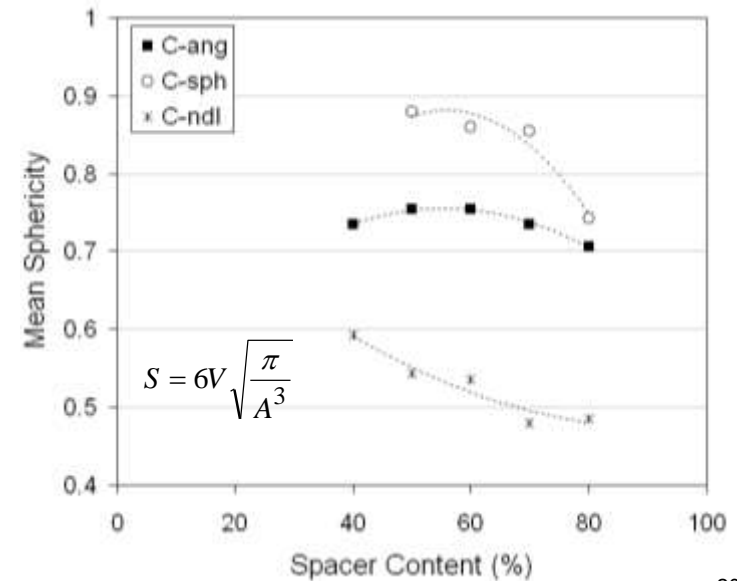
ON

**ARCHITECTURAL & MECHANICAL
PROPERTIES**

PORE MORPHOLOGY



Plot removed due to copyright restrictions. See Figure 3: Tuncer, N., et al. "Influence of Cell Aspect Ratio on Architecture and Compressive Strength of Titanium Foams". *Materials Science and Engineering A* 528 (2011): 7368-74.



Source: Tuncer, N., G. Arslan, et al. "Influence of Cell Aspect Ratio on Architecture and Compressive Strength of Titanium Foams." *Materials Science and Engineering A* 528 (2011): 7368-74. Courtesy of Elsevier. Used with permission.

PORE MORPHOLOGY – DEFORMATION MECHANISM

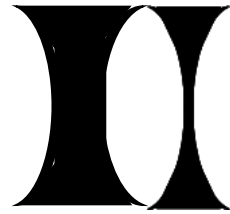
C-ndl



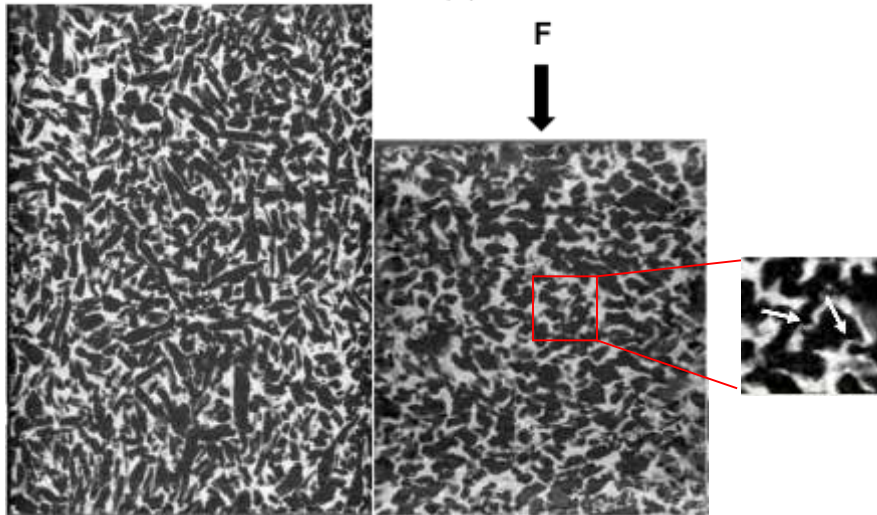
C-ang



C-sph

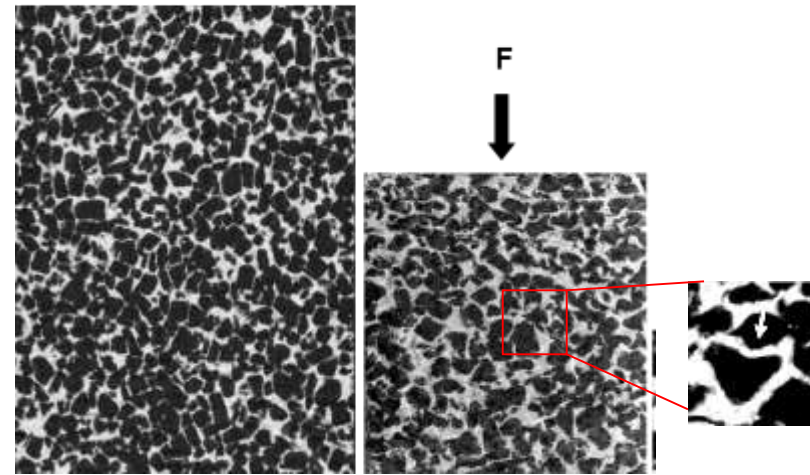


C-ndl
(a)



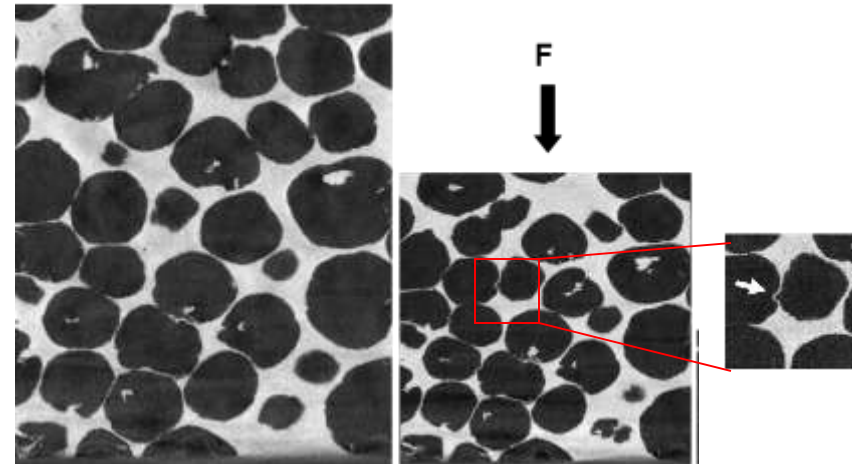
C-ang

(b)



C-sph

(c)



Source: Tuncer, N., G. Arslan, et al. "Influence of Cell Aspect Ratio on Architecture and Compressive Strength of Titanium Foams." *Materials Science and Engineering A* 528 (2011): 7368– 74. Courtesy of Elsevier. Used with permission.

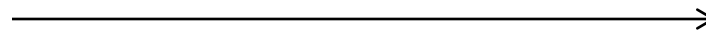
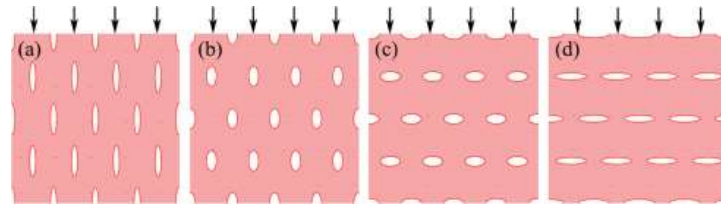
PORE MORPHOLOGY – MECHANICAL PROPERTIES

Plot removed due to copyright restrictions. See Figure 6: Tuncer, N., et al. "Influence of Cell Aspect Ratio on Architecture and Compressive Strength of Titanium Foams". *Materials Science and Engineering A* 528 (2011): 7368-74.

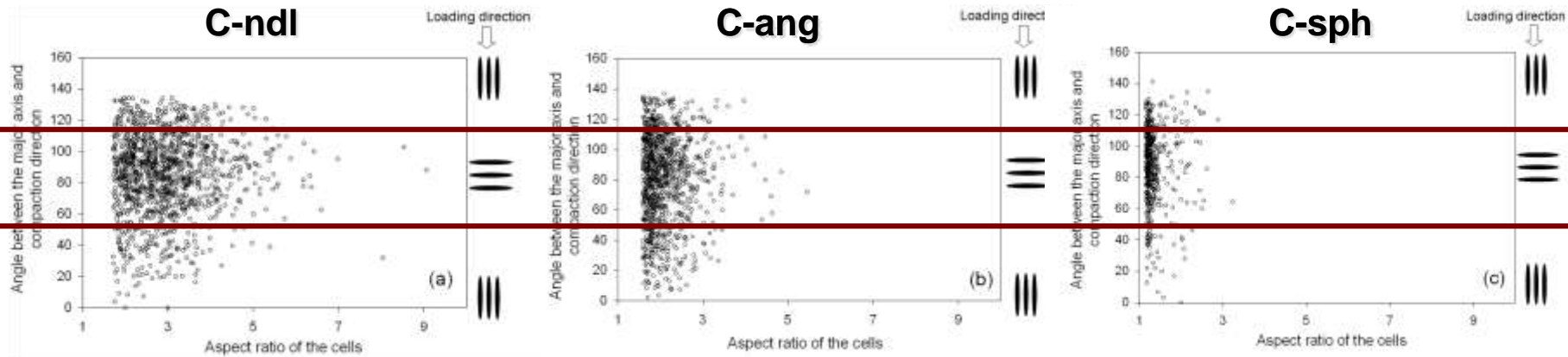
High aspect ratio pores result in lower strength at the same porosity

$$\frac{\sigma^*}{\sigma_s} = 1.017 \left(\frac{\rho^*}{\rho_s} \right)^{1.5} - 0.018A - 0.091 \quad R^2 = 0.977$$

PORE MORPHOLOGY



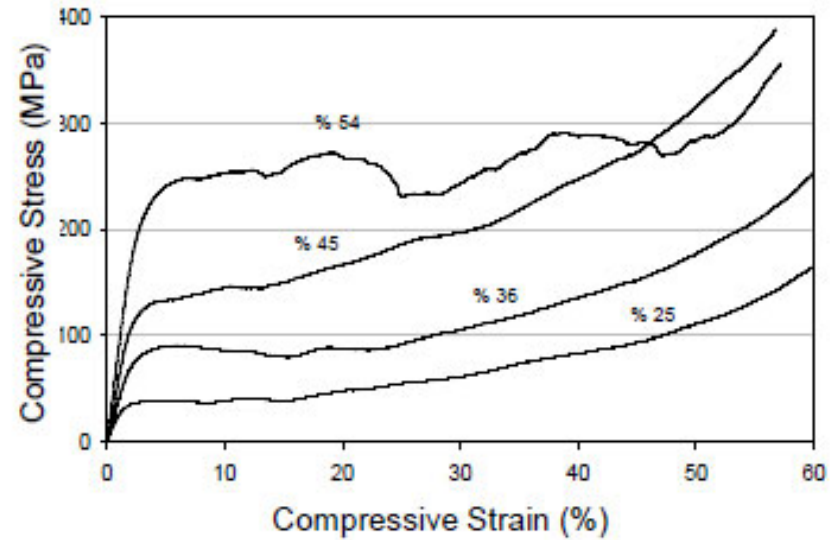
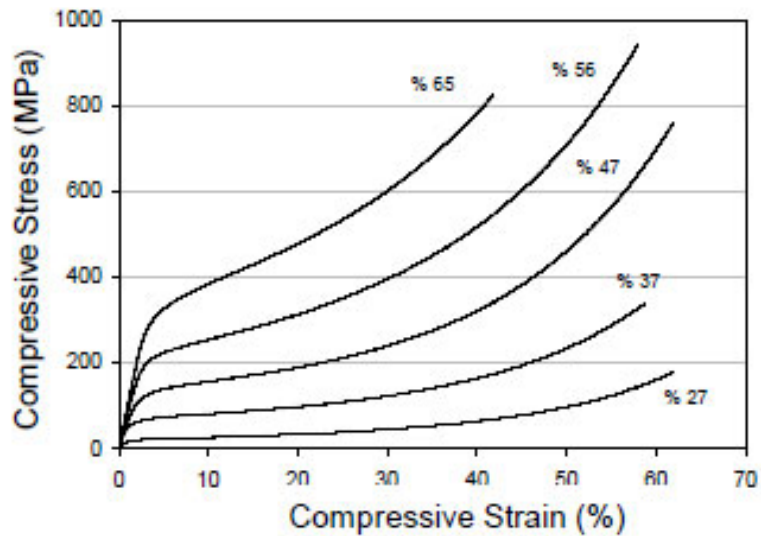
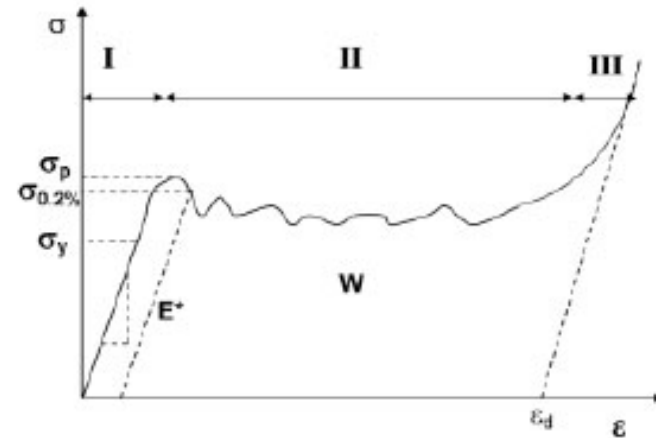
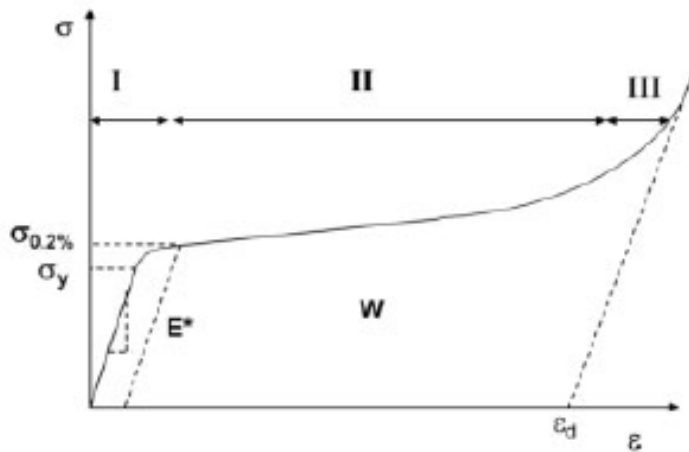
Strength decreases



Source: Tuncer, N., et al. "Influence of Cell Aspect Ratio on Architecture and Compressive Strength of Titanium Foams". *Materials Science and Engineering A* 528 (2011): 7368–74. © Elsevier / Science Direct. All rights reserved. This content is excluded from our Creative Commons license. For more information, see <http://ocw.mit.edu/help/faq-fair-use/>.

PORE MORPHOLOGY

Plateau behavior



Small angular pored foams

Large spherical pored foams

Source: Tuncer, Nihan. "Structure-property Relationship in Titanium Foams", PhD dissertation, Anadolu University, Turkey, 2011.

COLLAPSE MODES IN FOAMS

Cell-wall buckling

Layer-wise collapse perpendicular to the loading direction



Oscillations in stress-strain diagram

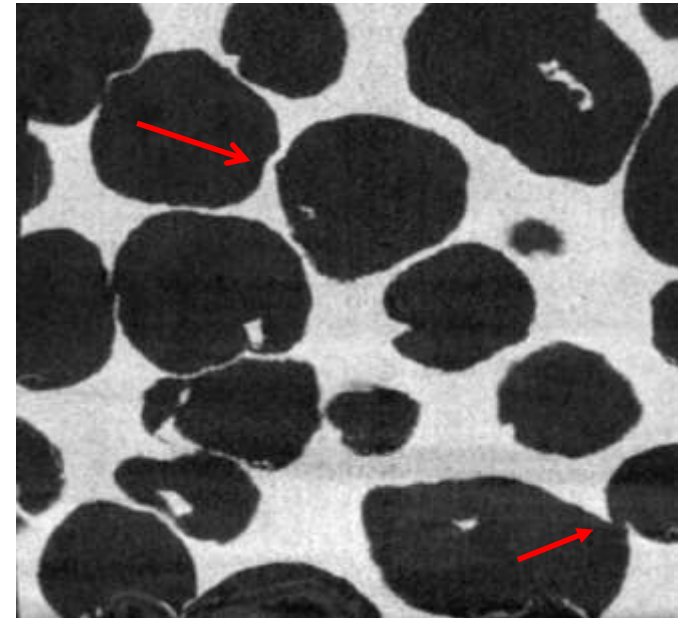
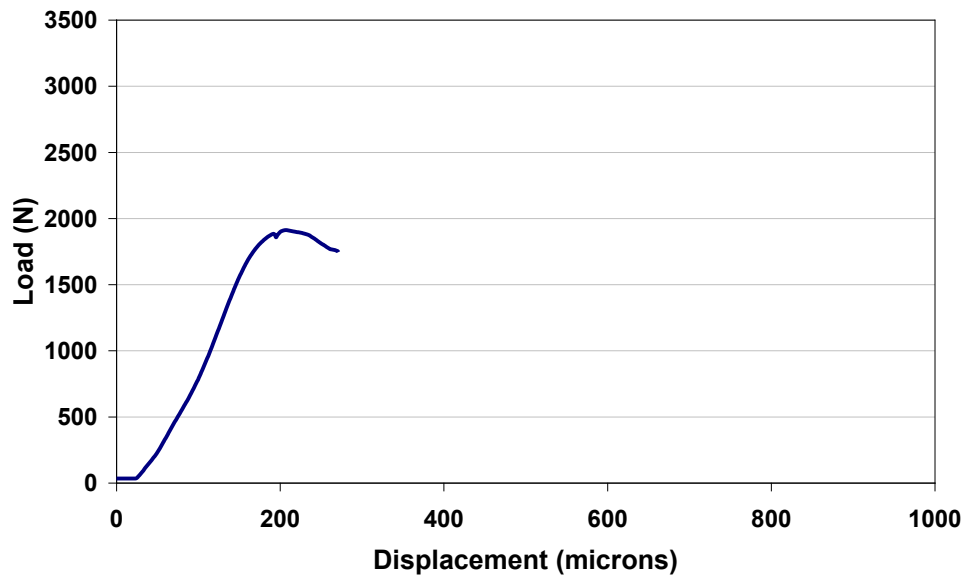
Cell-wall bending

Shear localisation occurs.
Deformation at nearly constant applied stress by shear bands



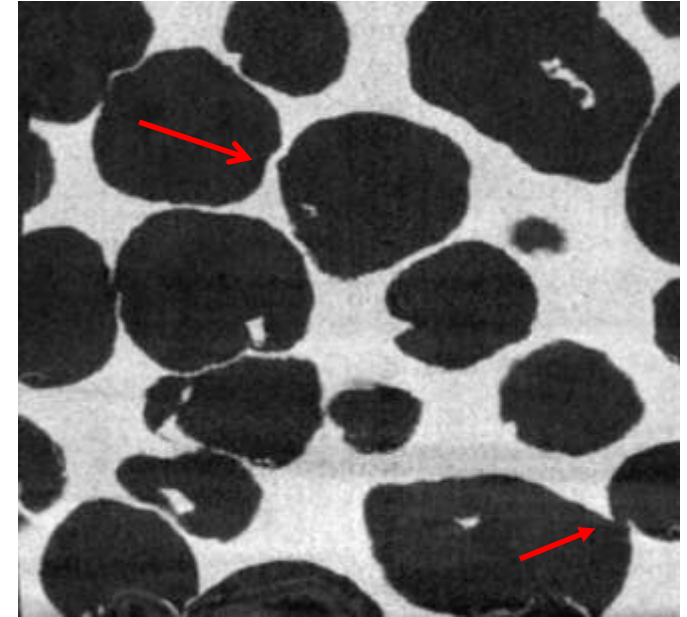
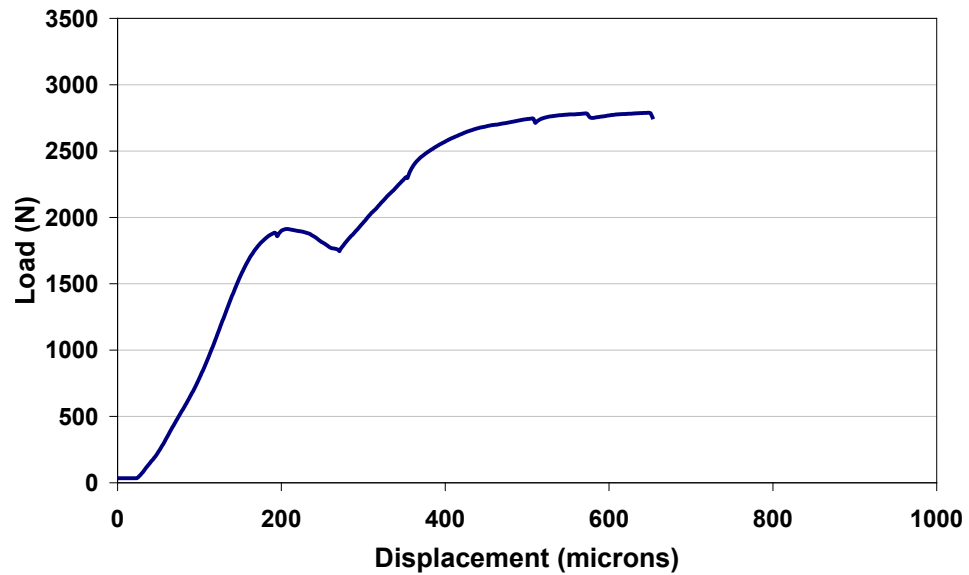
Smooth stress-strain diagram

PORE MORPHOLOGY



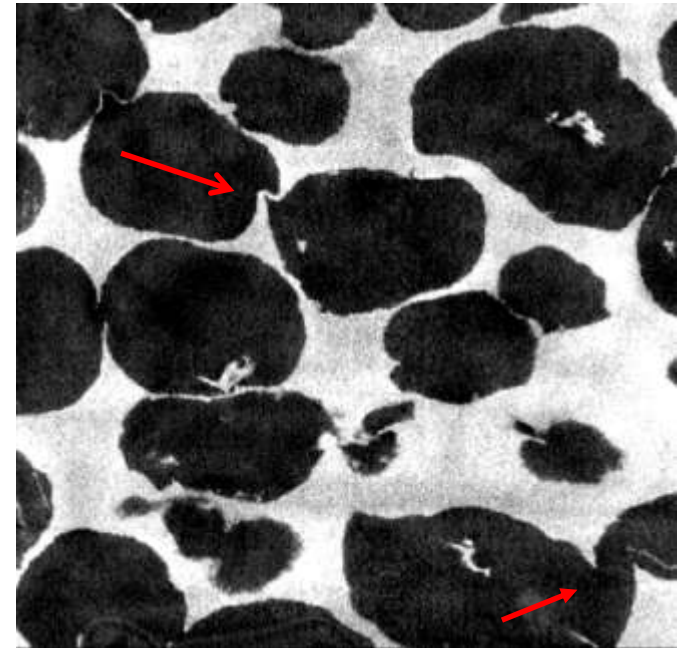
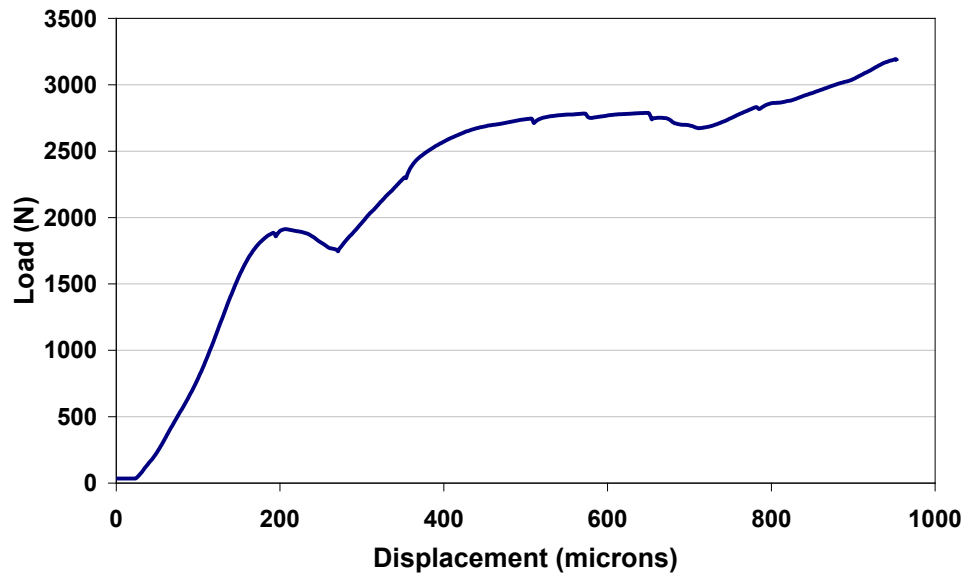
Source: Tuncer, Nihan. "Structure-property Relationship in Titanium Foams", PhD dissertation, Anadolu University, Turkey, 2011.

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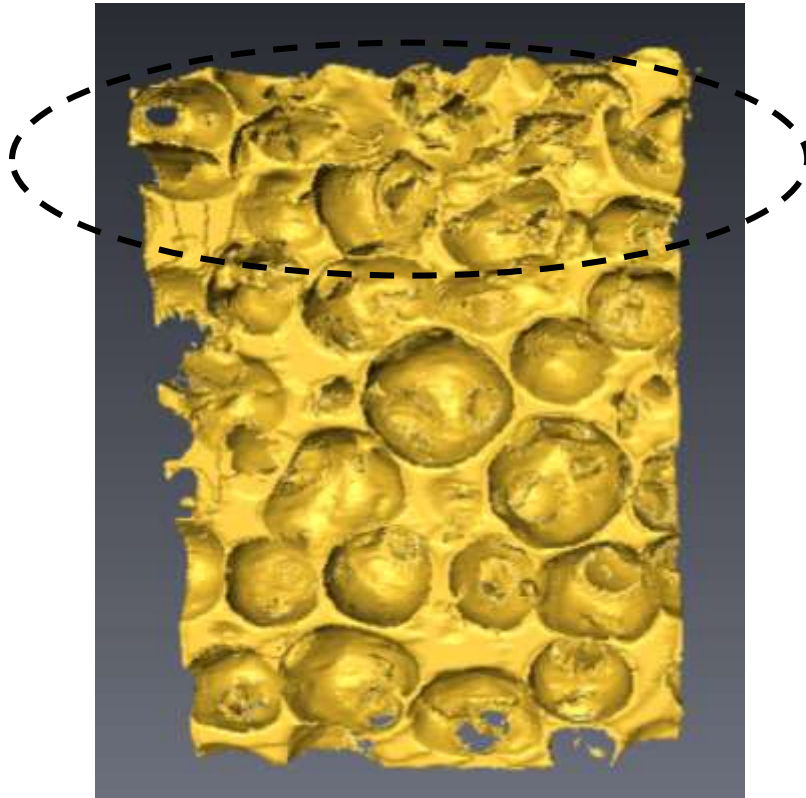
Source: Tuncer, Nihan. "Structure-property Relationship in Titanium Foams", PhD dissertation, Anadolu University, Turkey, 2011.

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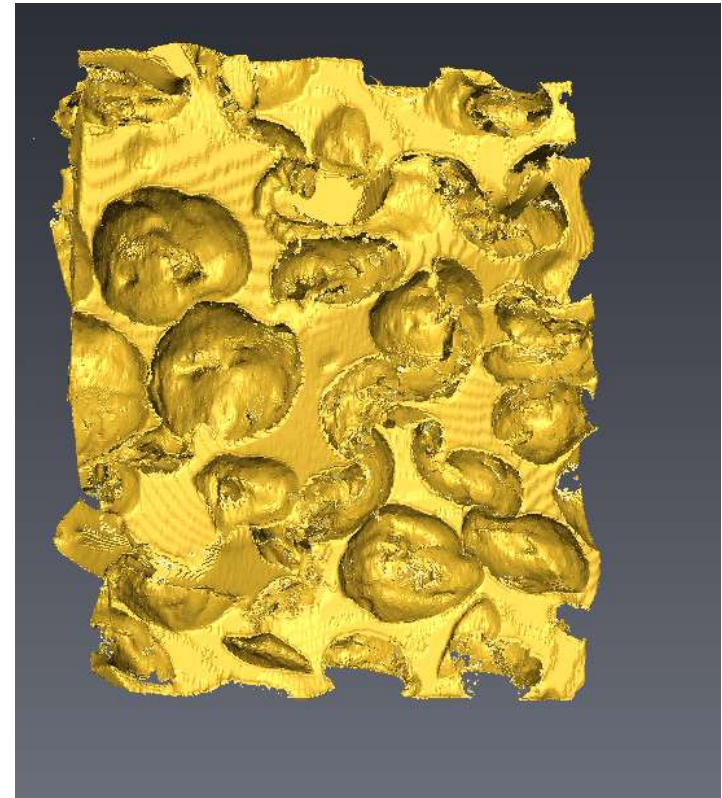


Source: Tuncer, Nihan. "Structure-property Relationship in Titanium Foams", PhD dissertation, Anadolu University, Turkey, 2011.

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After the yield point

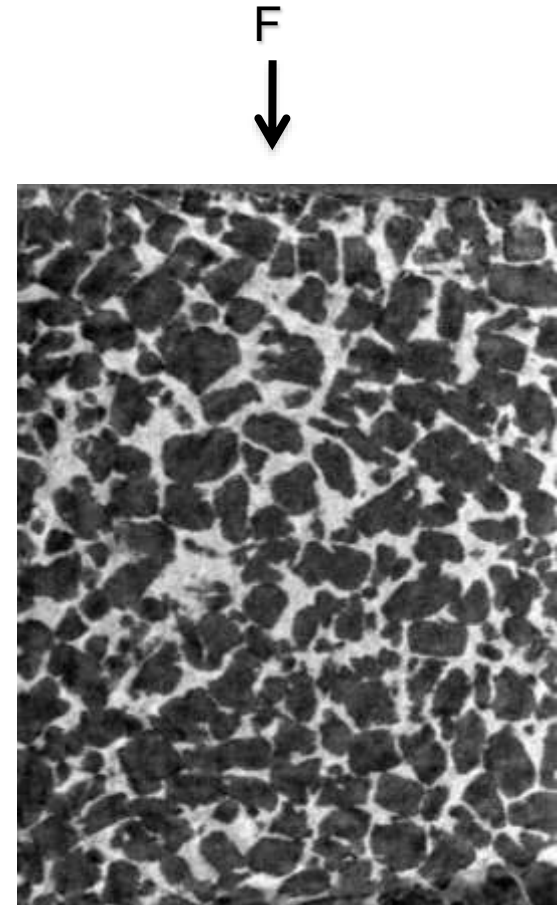
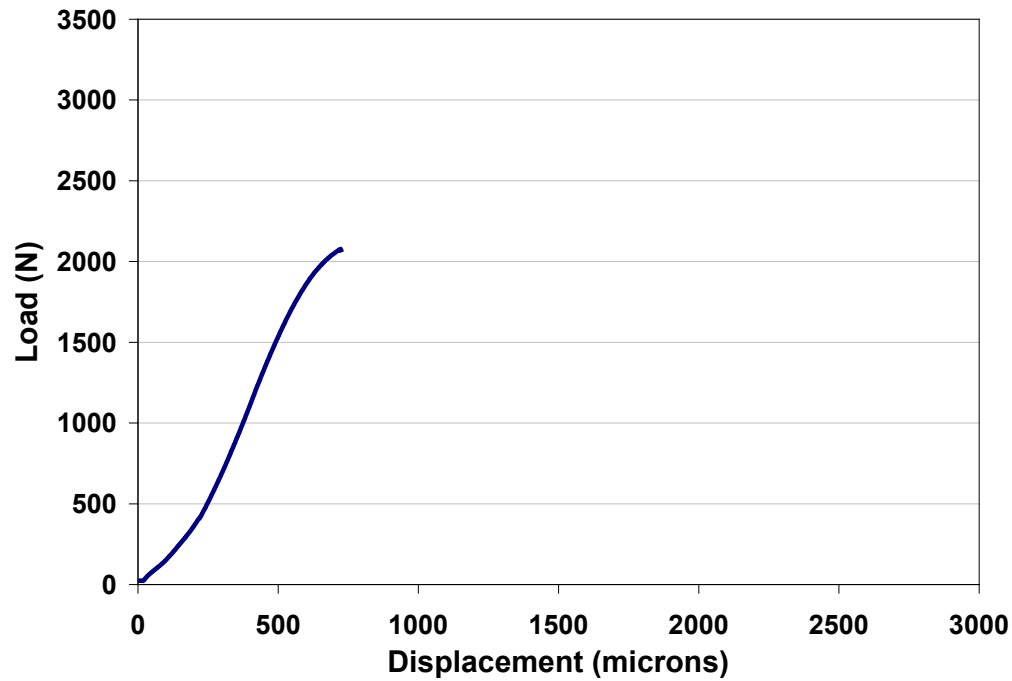


Final state (severe deformation)

Layer-wise collapse in the early stages of deformation

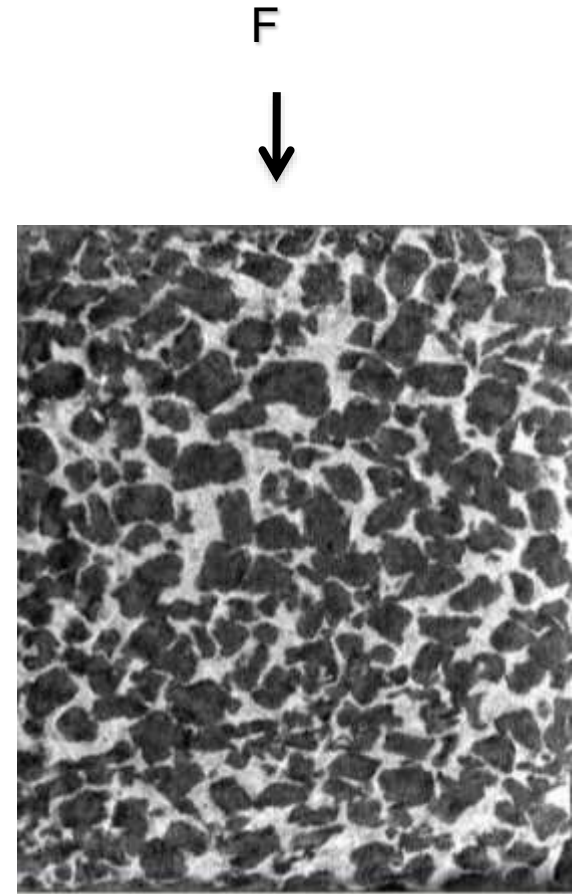
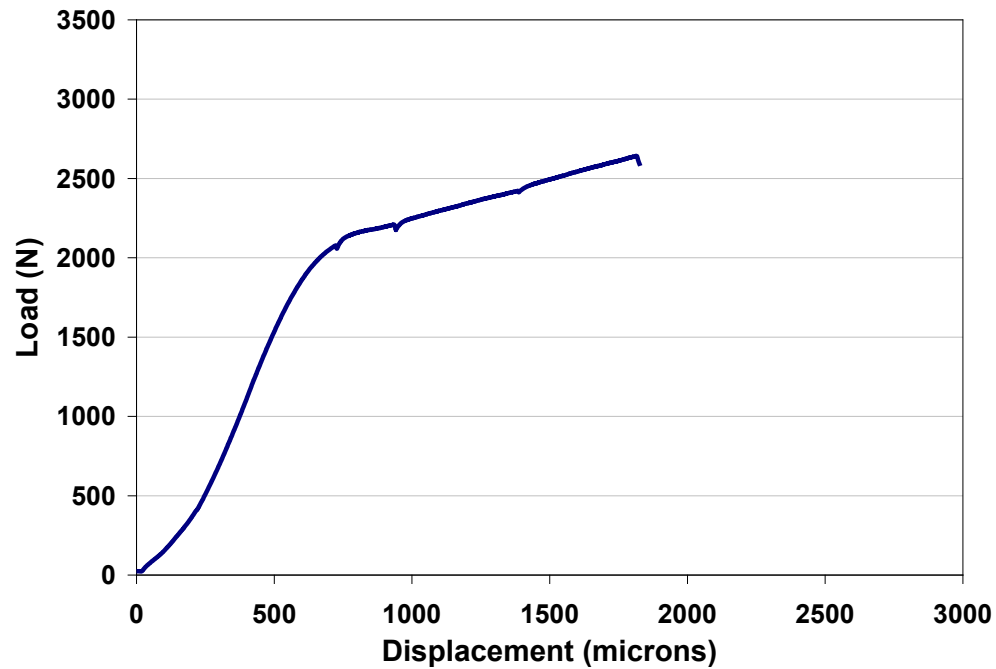
Source: Tuncer, Nihan. "Structure-property Relationship in Titanium Foams",
PhD dissertation, Anadolu University, Turkey, 2011.

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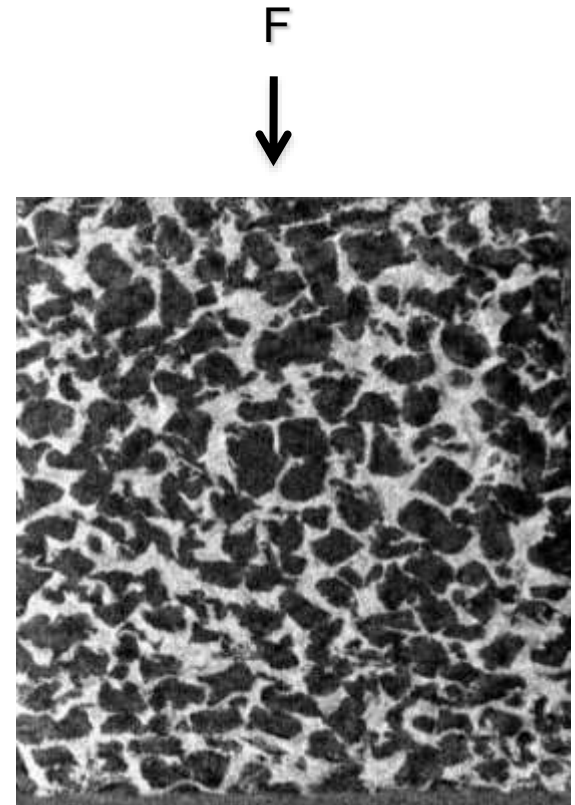
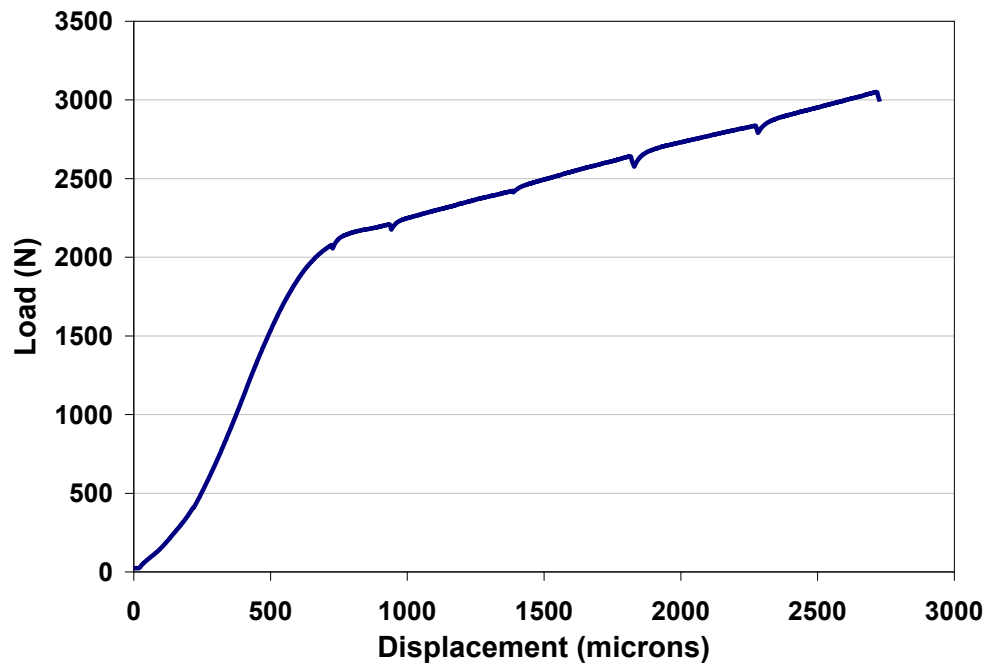
Source: Tuncer, Nihan. "Structure-property Relationship in Titanium Foams", PhD dissertation, Anadolu University, Turkey, 2011.

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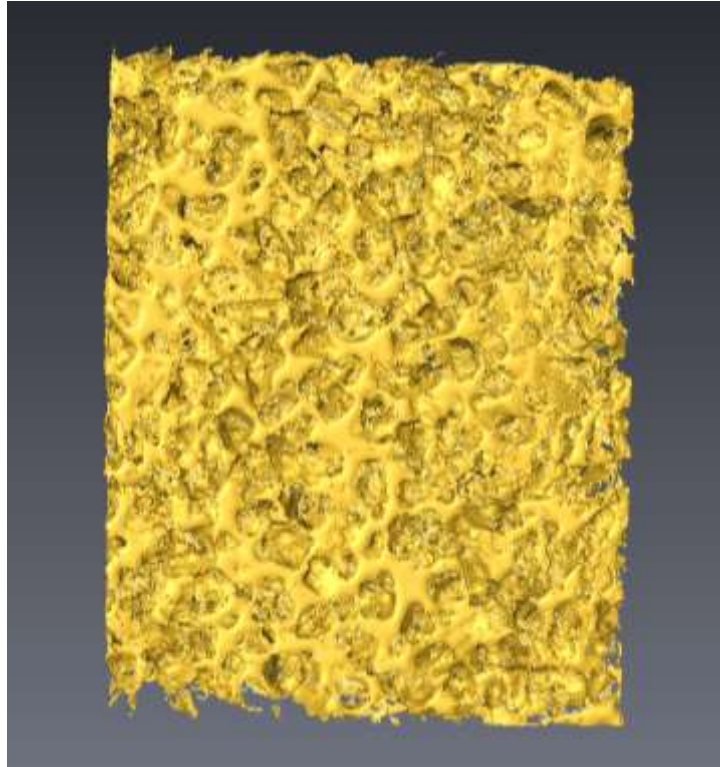
Source: Tuncer, Nihan. "Structure-property Relationship in Titanium Foams", PhD dissertation, Anadolu University, Turkey, 2011.

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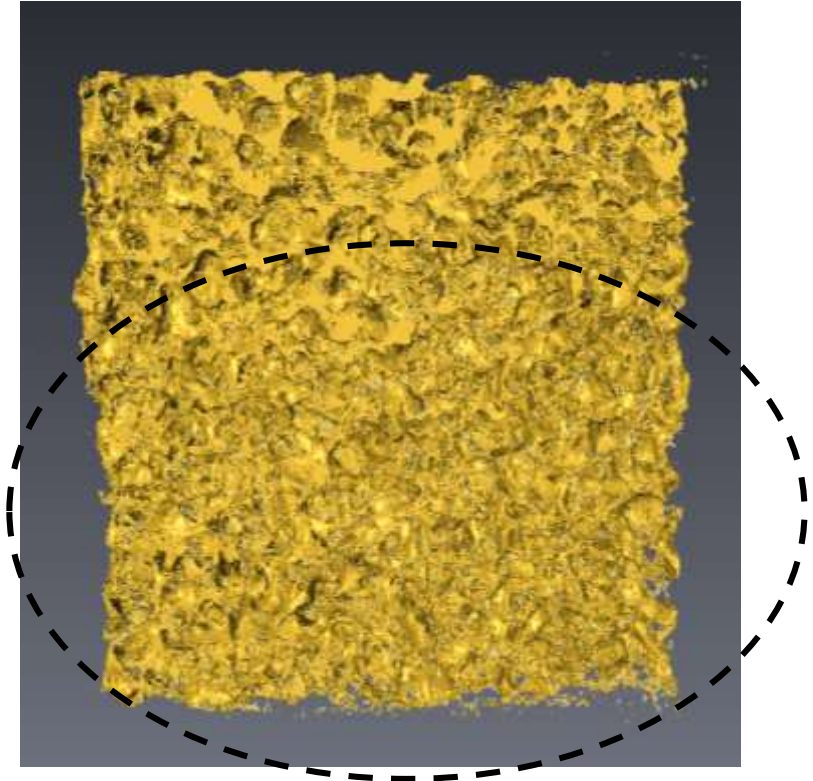


Source: Tuncer, Nihan. "Structure-property Relationship in Titanium Foams", PhD dissertation, Anadolu University, Turkey, 2011.

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1st step after yield



Final step (severe deformation)

A more homogeneous deformation

Source: Tuncer, Nihan. "Structure-property Relationship in Titanium Foams",
PhD dissertation, Anadolu University, Turkey, 2011.

CONCLUSIONS

Random foams deviate from well known models due to imperfections that form during processing. Processing parameters should be watched carefully to address the property variations.

Large and low aspect ratio pores enhance compressive strength at the same relative density.

Dominant collapse mechanism in needle-like-pored foams is buckling whereas in angular-pored foams it's cell wall bending.

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