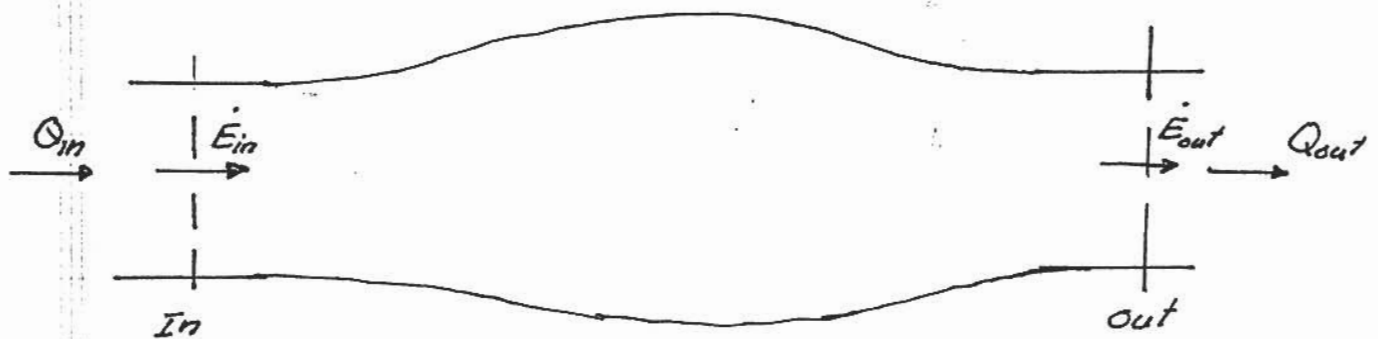


## LECTURE # 13

### 1.060 ENGINEERING MECHANICS II

#### CONSERVATION OF MECHANICAL ENERGY



$\dot{E}$  = flow rate of mechanical energy across flow area  $A$  where flow is well behaved =  $\rho g Q H$

$$\left. \begin{aligned} \sum \dot{E}_{in} - \sum \dot{E}_{out} \\ \sum (\rho g Q_{in} H_{in}) - \sum (\rho g Q_{out} H_{out}) \end{aligned} \right\} \begin{array}{l} \text{Net rate of Dissipation of} \\ \text{Mechanical Energy within CV} \end{array}$$

Similar to momentum principle: Knowledge of in- and outflow conditions quantifies what's going on inside without us knowing the details

It only one inflow & one outflow area, then  $Q_{in} = Q_{out}$  from volume conservation (Steady)

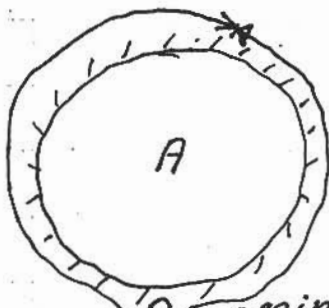
$$\rho g Q H_{in} - \rho g Q H_{out} = \dot{E}_{diss}$$

or

$$H_{in} - H_{out} = \frac{\dot{E}_{diss}}{\rho g Q} = \text{Head Loss} = \Delta H_{1-2}$$

If loss is due to friction along stream tube walls, we have from Momentum (Lecture #12)

$$H_1 - H_2 = H_{in} - H_{out} = \int_{s_1}^{s_2} \frac{\tau_s P}{\rho g A} ds = \Delta H_f$$



$P$  = perimeter of solid-fluid contact

$$\tau_s P = \int \tau dP$$

but if  $\tau_s P = \text{constant}$ , as it would be for a circular pipe, and if  $A$  is uniform, then  $\tau_s P$ , and  $A$  are constants - and

$$\Delta H_f = \text{frictional head loss} = \frac{\tau_s P (s_2 - s_1)}{\rho g A}$$

This has a very "nice" physical interpretation.

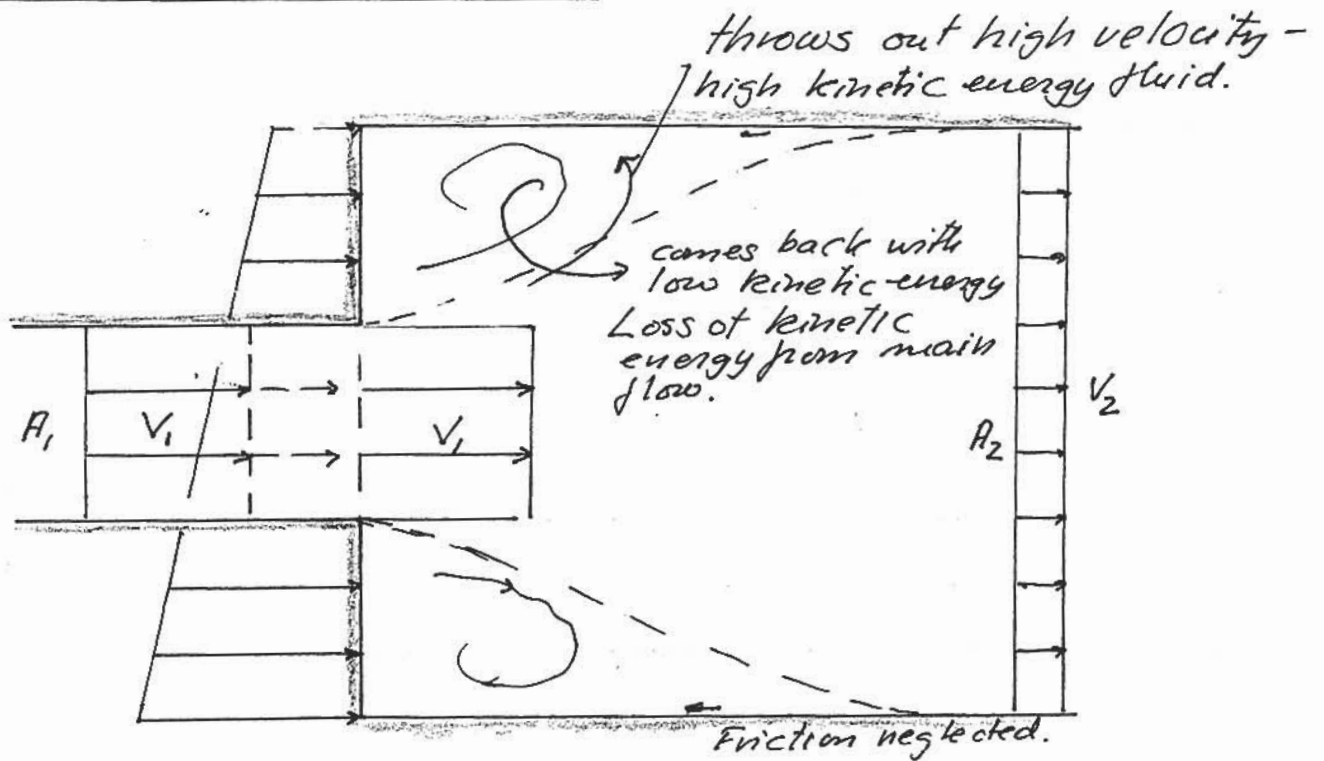
$\rho g Q \Delta H_f$  = rate of dissipation of Mech. Energy due to friction along walls over a length of pipe  $(s_2 - s_1) = \rho g Q \tau_s P (s_2 - s_1) / (\rho g A)$ .

but  $V = Q/A$ , so

$$\dot{E}_{diss, f} = \underbrace{[\tau_s P (s_2 - s_1)]}_{\substack{\text{shear stress} \\ \text{area upon} \\ \text{which } \tau_s \text{ acts}}} \cdot \underbrace{V}_{\substack{\text{average} \\ \text{velocity}}} = \text{Rate of Work Done to overcome FRICTION.}$$

{ Total frictional force resisting the movement } · { Velocity }

## EXPANSION HEADLOSS



Continuity :  $Q = V_1 A_1 = V_2 A_2$   
 $+ \rho \cdot 0 \cdot (A_2 - A_1)$

Momentum :  $\rho V_1^2 A_1 + p_1 [A_1 + (A_2 - A_1)] =$

$\rho V_1^2 A_1 + p_1 A_2 = \rho V_2^2 A_2 + p_2 A_2$  or

$(p_1 - p_2) A_2 = \rho (V_2 A_2) V_2 - \rho (V_1 A_1) V_1 = \rho V_2 A_2 (V_2 - V_1)$   
 $\dot{Q} = V_1 A_1 = \dot{Q}$

$H_1 - H_2 = \frac{p_1 - p_2}{\rho g} + \frac{V_1^2 - V_2^2}{2g} + \frac{z_1 - z_2}{0} = \Delta H_{exp}$

$\Delta H_{exp} = \frac{2V_2(V_2 - V_1)}{2g} + \frac{V_1^2}{2g} - \frac{V_2^2}{2g} = \frac{V_2^2 - 2V_2V_1 + V_1^2}{2g} = \frac{(V_1 - V_2)^2}{2g}$

## GENERALIZED BERNOULLI EQUATION

$$H = \text{Total Head} = K_e \frac{V^2}{2g} + \frac{p}{\rho g} + z$$

is defined only for flow that is well behaved, i.e.

$$K_e \approx K_m \approx 1$$

$$V = Q / A$$

$p$  = pressure at center of gravity of  $A$

$z$  = elevation of center of gravity of  $A$

$$H_1 - H_2 = \Delta H$$

$H_1$  = "upstream",  $H_2$  = "downstream" total head

Flow is from ① → ②

$\Delta H \geq 0$  = head loss from ① to ②

$$\Delta H = \Delta H_f + \Delta H_{exp}$$

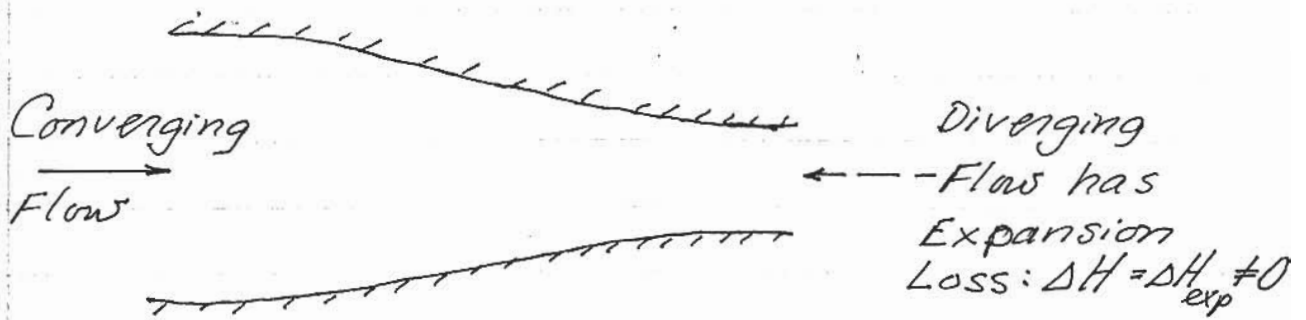
$$\Delta H_f = \text{frictional head loss} = \int_1^2 \frac{\tau_s p}{\rho g A} ds$$

$$\Delta H_{exp} = \text{expansion head loss} = \frac{(\Delta V)^2}{2g}$$

When does  $\Delta H \approx 0$ , i.e.  $H_1 = H_2$  Work?

"Short" Transition of "Converging" Flow

"Converging" flow means that the velocity in the direction of flow is increasing.



$\Delta H \approx 0$  if the convergence (transition) is "short". "Short" means that frictional headloss can be considered negligible.

$$\Delta H_f \approx \frac{f}{4} \left( \frac{Pl_{12}}{A} \right) \frac{V^2}{2g} \ll \frac{V^2}{2g} \text{ then } \Delta H_f \approx 0$$

With  $f \approx 0.02$  and "circular" crosssections this translates to an approximate condition of

$$l_{12} = \text{length of streamline} \approx \text{length of transition} \ll 50 D$$

where  $D$  is linear dimension of the flow area.

SOME EXAMPLES

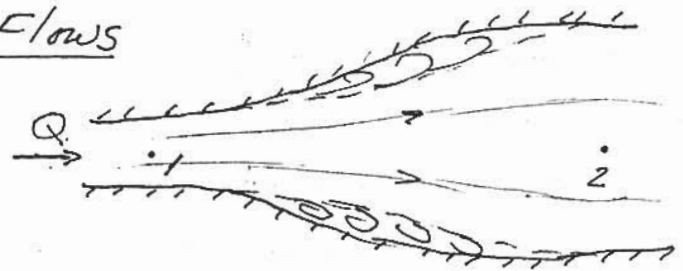
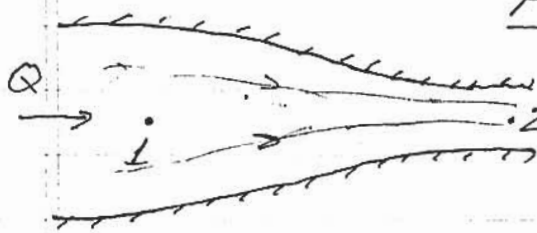
$H_1 = H_2$  OK

$H_1 \neq H_2$

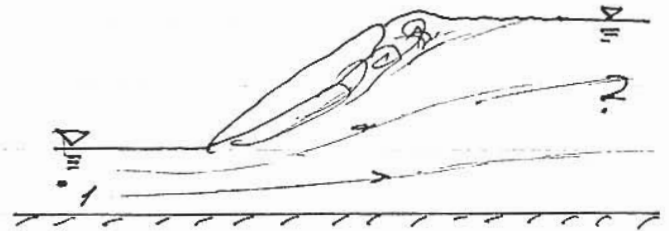
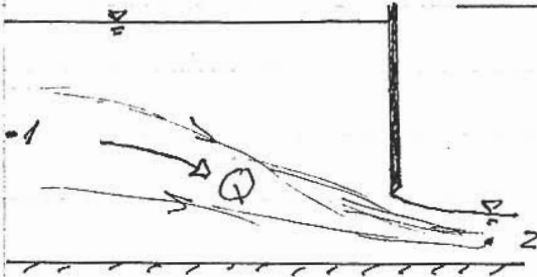
Converging Flows

Diverging Flows

Pipe Flows



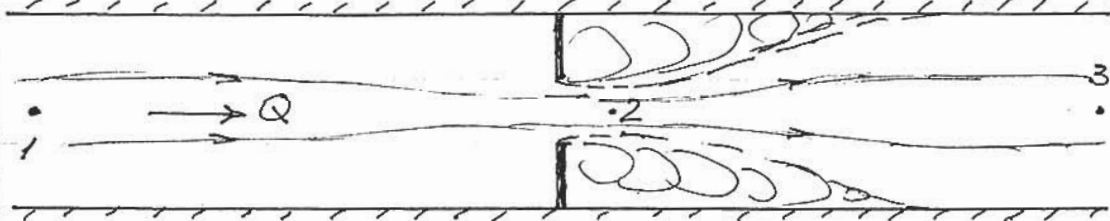
Channel Controls



Orifice Meter in Pipe

$H_1 = H_2$

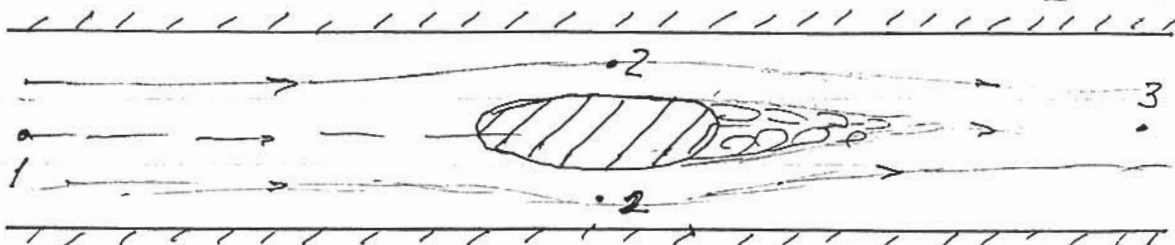
$H_2 \neq H_3$



$H_1 = H_2$

Flow around Body

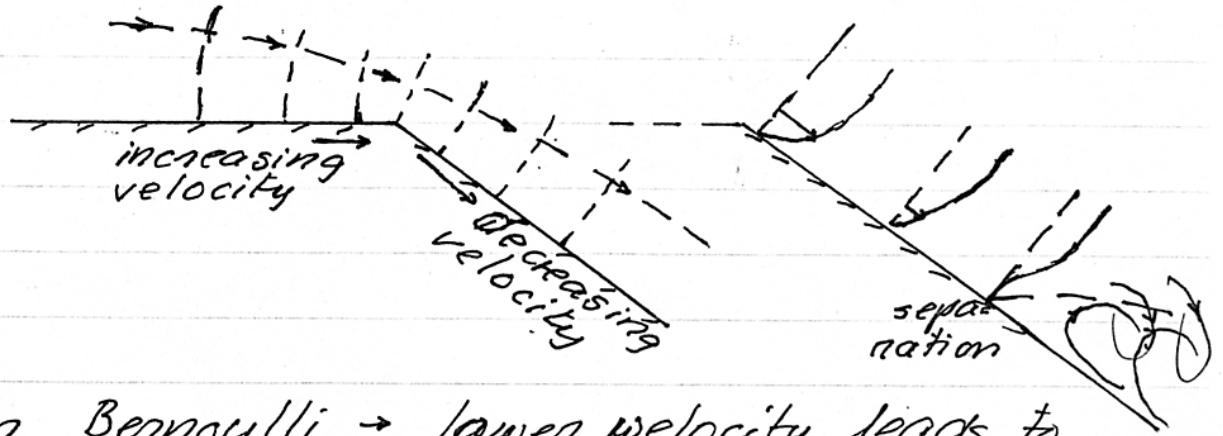
$H_2 \neq H_3$



When does  $\Delta H \approx 0$  NOT Work?

"Expanding" Flow, even if Transition is "Short"

"Expanding" flow mean that the velocity in the direction of flow is decreasing.



From Bernoulli  $\rightarrow$  lower velocity leads to higher pressure!

As fluid particle is moving "against" a pressure gradient that slows it down the particle will be stopped and turned around unless it had enough momentum when it encountered the "adverse" pressure gradient. For a real fluid the velocity near a solid boundary is very low (no-slip condition) and its momentum is therefore low and it does not take much to turn it around. The flow separates from the boundary creating an eddy of low velocity swirling fluid that extracts energy from the main flow and causes a HEADLOSS