

Integral Boundary Layer Equations

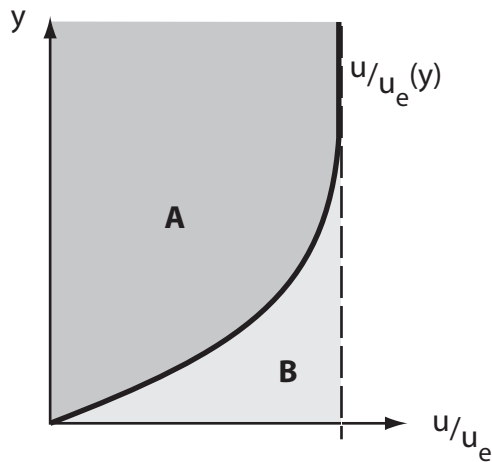
Displacement Thickness

The displacement thickness δ^* is defined as:

$$\delta^* = \underbrace{\int_0^\infty \left(1 - \frac{\rho u}{\rho_e u_e}\right) dy}_{\text{compressible flow}} = \underbrace{\int_0^\infty \left(1 - \frac{u}{u_e}\right) dy}_{\text{incompressible flow}}$$

The displacement thickness has at least two useful interpretations:

Interpretation #1



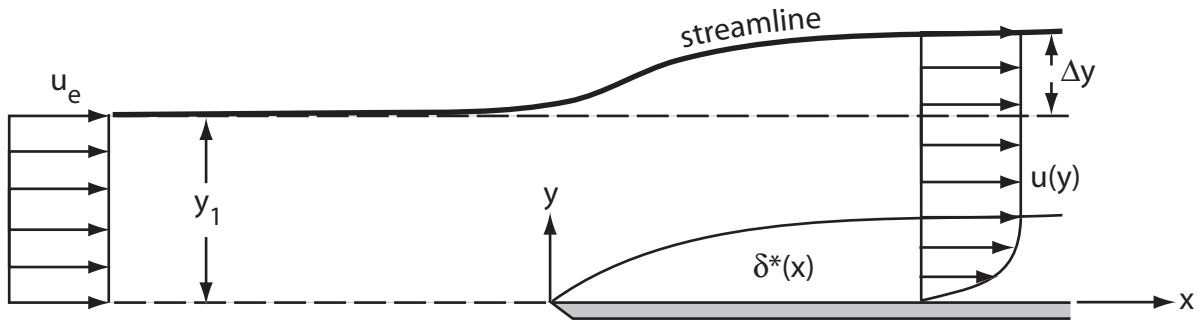
$$\mathbf{A} = \int_0^\infty \frac{u}{u_e} dy$$

$$\mathbf{A} + \mathbf{B} = \int_0^\infty (1) dy$$

So, the difference is in area **B**.

$\Rightarrow \delta^*$ “represents” the decrease in mass flow due to viscous effects, i.e. lost

$$\dot{m}_{\text{visc}} = \rho_e u_e \delta^*$$

Interpretation #2

Conservation of mass:

$$\int_0^{y_1} u_e dy = \int_0^{y_1 + \Delta y} u dy$$

$$\int_0^{y_1} u_e dy = \int_0^{y_1} u dy + \Delta y u_e$$

$$\Rightarrow \Delta y u_e = \int_0^{y_1} (u_e - u) dy$$

$$\Delta y = \int_0^{y_1} \left(1 - \frac{u}{u_e}\right) dy$$

Taking the limit of $y_1 \rightarrow \infty$ gives

$$\Rightarrow \Delta y = \delta^* = \int_0^{\infty} \left(1 - \frac{u}{u_e}\right) dy$$

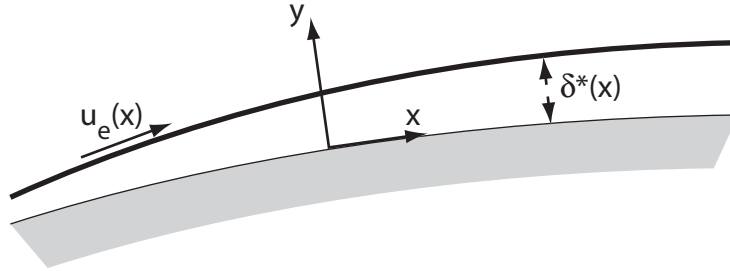
So, the external streamline is displaced by a distance δ^* away from the body due to viscous effects.

\Rightarrow Outer flow sees an “effective body”

Karman's Integral Momentum Equation

This approach due to Karman leads to a useful approximate solution technique for boundary layer effects. It forms the basis of the boundary layer methods utilized in Prof. Drela's XFOIL code.

Basic idea: integrate b.l. equations in y to reduce to an ODE in x .



Derivation:

Add (ρu) x continuity + x - momentum

$$\begin{aligned} \Rightarrow \underbrace{\rho u \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right)}_{(\rho u) \times \text{continuity}} + \underbrace{\rho \left(u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right)}_{x\text{-momentum}} &= \rho u_e \frac{du_e}{dx} + \mu \frac{\partial^2 u}{\partial y^2} \\ \Rightarrow \rho \left(\frac{\partial(u^2)}{\partial x} + \frac{\partial}{\partial y}(uv) \right) &= \rho u_e \frac{du_e}{dx} + \frac{\partial}{\partial y} \left(\underbrace{\mu \frac{\partial u}{\partial y}}_{\tau} \right) \end{aligned}$$

Now, we integrate from 0 to y_1 :

$$\rho \int_0^{y_1} \frac{\partial(u^2)}{\partial x} dy + \rho uv \Big|_0^{y_1} = \rho u_e \frac{du_e}{dx} y_1 + \tau \Big|_0^{y_1}$$

Note:

$$\rho uv \Big|_0^{y_1} = \rho u_e v(y_1) = \rho u_e \int_0^{y_1} \frac{\partial v}{\partial y} dy = -\rho u_e \int_0^{y_1} \frac{\partial u}{\partial x} dy$$

So, the equation becomes:

$$\rho \int_0^{y_1} \frac{\partial(u^2)}{\partial x} dy - \rho u_e \int_0^{y_1} \frac{\partial u}{\partial x} dy = \rho u_e \frac{du_e}{dx} y_1 + \tau_w \Big|_0^{y_1}$$

After a little more manipulation this can be turned into (note we let $y_1 \rightarrow \infty$ also):

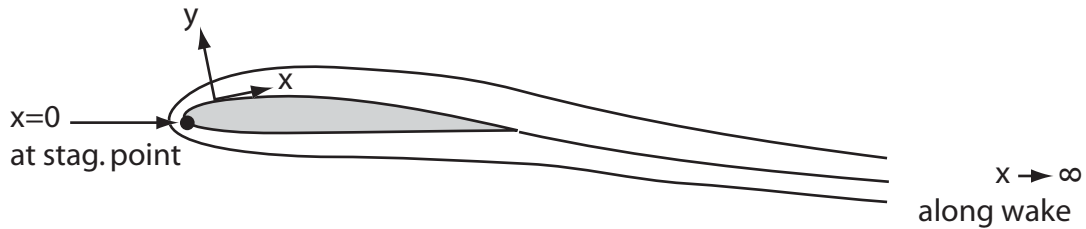
$$\tau_w = \frac{d}{dx} (\rho u_e^2 \theta) + \rho u_e \delta^* \frac{du_e}{dx} \quad (1)$$

where $\theta \equiv$ momentum thickness $= \int_0^{\infty} \frac{\rho u}{\rho_e u_e} \left(1 - \frac{\rho u}{\rho_e u_e}\right) dy$

incompressible form $= \int_0^{\infty} \frac{u}{u_e} \left(1 - \frac{u}{u_e}\right) dy$

Insight

Integrate (1) from stagnation point along airfoil & then down the wake



$$\int_0^{\infty} \tau_w dx = (\rho u_e^2 \theta) \Big|_0^{\infty} + \int_0^{\infty} \rho u_e \delta^* \frac{du_e}{dx} dx$$

But: $u_e = 0$ at stag. pt. ($x = 0$) & $\underbrace{-\frac{dp}{dx} = \rho u_e \frac{du_e}{dx}}_{\text{Bernoulli}}$

$$\Rightarrow \underbrace{\rho u_e^2 \theta \Big|_{x \rightarrow \infty}}_{\text{drag (see Anderson Sec 2.6 for proof)}} = \int_0^{\infty} \tau_w dx + \int_0^{\infty} \delta^* \frac{dp}{dx} dx$$

$$D' = \underbrace{\int_0^{\infty} \tau_w dx}_{\text{friction drag}} + \underbrace{\int_0^{\infty} \delta^* \frac{dp}{dx} dx}_{\text{form drag}}$$

Another common form of the integral momentum equation is derived below:

$$\tau_w = \frac{d}{dx}(\rho_e u_e^2 \theta) + \rho_e u_e \delta^* \frac{du_e}{dx}$$

$$\frac{\tau_w}{\rho_e u_e^2} = \frac{d\theta}{dx} + \frac{\theta}{u_e} (2 + H) \frac{du_e}{dx}$$

where

$$H = \frac{\delta^*}{\theta} \leftarrow \text{known as "shape parameter"}$$